

SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered) **READ INSTRUCTIONS** REPORT DOCUMENTATION PAGE BEFORE COMPLETING FORM 2. GOVT ACCESSION NO. 3 RECIPIENT'S CATALOG NUMBER WHO1-78-49 YPE OF REPORT A PERIOD COVERED COMPILATION OF MOORED CURRENT METER DATA AND SSOCIATED OCEANOGRAPHIC OBSERVATIONS VOLUME Technical XVII9 POLYMODE ARRAY II DATA NØØØ14-74-C-Ø262? Susan/Tarbell, Ann/Spencer and Richard E./Payne N00014-76-C-01975 OCE 75 - 03962 PERFORMING ORGANIZATION NAME AND ADDRESS PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Woods Hole Oceanographic Institution ' 000 NR 083-004 Woods Hole, MA 02543 NR 083-400 11 CONTROLLING OFFICE NAME AND ADDRESS Jul 4-1978 NORDA National Space Technology Laboratory Bay St. Louis. MS 39529
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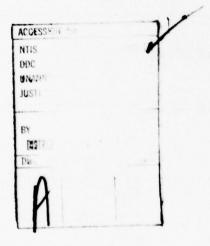
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Low passed east and north current components, temperature and pressure from current meters and temperature/pressure recorders are displayed graphically and in tabular form. Spectral diagrams are plotted for temperature and the vector components when a continuous two year time series was achieved. Progressive vector plots are included for velocity data.

Selected CTD data are presented as potential temperature and salinity values plotted against pressure.

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WHOI-78-49

A COMPILATION OF MOORED CURRENT METER DATA AND ASSOCIATED OCEANOGRAPHIC OBSERVATIONS, VOLUME XVII (POLYMODE ARRAY II DATA)

by

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July 1978

TECHNICAL REPORT

Prepared for the Office of Naval Research under Contract N00014-74-C-0262, NR 083-004; N00014-76-C-0197, NR 083-400 and for the National Science Foundation under Grant OCE75-03962.

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Valentine Worthington, Chairman Department of Physical Oceanography

ABSTRACT

Summaries of observations from moored stations and CTD profiles taken during POLYMODE Array II are presented. Data series of twenty-seven months duration at 12 locations were achieved with 3 consecutive deployments. Current meters were set at nominal depths of 600, 1000, 1500 and 4000 meters at eight of the locations and at 4000 meters at the remainder. Nine data series of eight months duration were obtained at similar depths at 3 additional locations.

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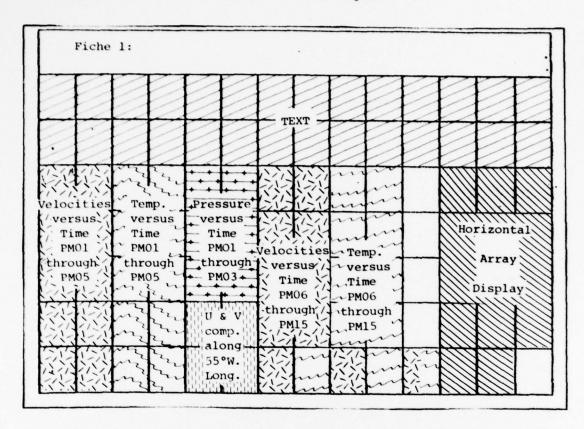
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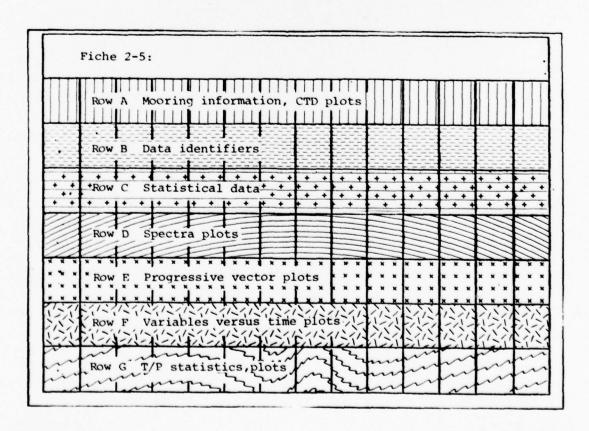
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Many people should share the credit for the excellent data return and the quality of data obtained during the POLYMODE Array II experiment, in particular the people in the buoy group instrument shop and those who worked on the moorings, both hardware and design. The officers and crews of the R. V. Knorr and R. V. Chain deserve special mention for their willing assistance in mooring deployment and recovery. The Principal Investigator for the POLYMODE Array II experiment is Dr. William J. Schmitz, Jr. The T/P data is courtesy of Dr. Carl Wunsch and the surface float tracks courtesy of Dr. Philip Richardson. CTD data were recorded and processed by the W.H.O.I. Physical Oceanography CTD Group.

The report was assembled with the help of Audrey Williams and data processors T. McKee and C. Mills and was reproduced at the M.I.T. Microreproduction Laboratory. The work was funded by Office of Naval Research Contract N00014-76-C-0262, NR 083-004; N00014-76-C-0197, NR 083-400 and National Science Foundation Grant IDO 75-03962.

PREFACE

This volume is the seventeenth in a series of Data Reports presenting moored current meter and associated data collected by the W.H.O.I. Buoy Group.

Volumes I through XVI present data from the years 1963-1971, and from several special experiments: the 1970 Pollard array, the 1973 IWEX array, the 1973 MODE array, the MODE Site moorings, and the Saint Croix mooring measurements.

Volume XVII presents data from POLYMODE Array II.

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XVI	78-5	Tarbell, S., and A. Spencer	1971-1975 MODE Site

Presentation

The entire report is presented on microfiche with the displays organized on the microfiche sheets by POLYMODE rather than W.H.O.I. mooring numbers as is usually our practice. W.H.O.I. vs. POLYMODE mooring numbers will be found in Table 1.

Except for the first two rows (A and B) in which the text is presented, microfiche sheet 1 displays composite plots of the data as an array.

Rows three (C) through seven (G) are arranged by columns as follows:

Columns 1 and 2	Velocity stick plots for POLYMODE moorings 1,2,3,4,5
Columns 3 and 4	Temperature plots for moorings 1,2,3,4,5
Columns 5 and 6	Pressure plots for moorings 1,2,3
Columns 5 and 6	East and north components, composites down 55°W
Columns 7 and 8	Velocity stick plots for moorings 6,7,8,9-12,13,14,15
Columns 9 and 10	Temperature plots for moorings 6,7,8,9-12,13,14,15
Columns 12,13,14	Velocity vectors plotted in seven day subsampled
	spatial arrays for 600, 1000, 1500, 4000 m depths

In the other microfiche sheets, the data from individual instrument locations are presented. Since instruments were reset at the same positions as closely as possible each location is represented by three records, one from each setting of the array. Each column on the microfiche represents an instrument location and each row contains a single data display type. These include:

- Row A Mooring information and CTD plots
- Row B Data identification (in large letters to permit unaided reading)
- Row C Statistical presentation
- Row D Spectra plots (presented for complete 2 year records)
- Row E Progressive vector plots
- Fow F Variables vs. time plots
- Row G $\,$ T/P statistics, variables vs. time, temperature spectra See Table 2 for a summary of depths and duration of the presented data.

Introduction

The POLYMODE program is an international cooperative scientific investigation of the dynamics and statistics of the mesoscale motions in the sea, the energy sources of these motions, and their contribution to the general circulation of the ocean. POLYMODE includes theoretical investigations, experiments, and field observations. Of the field observations, the largest is the statistical geographic experiment designed to determine the distribution of energy levels and space and time scales of the eddy field throughout the western North Atlantic using current meter arrays, SOFAR float arrays, and hydrographic and XBT work.

Three current meter arrays were set whose locations are shown in Fig. 1. Array I was set to define the statistics of the mesoscale motions to the east and north of the MODE-I site (28°N, 70°W) and to resolve the time length scales. Building on the results of MODE-I and POLYMODE Array I, Array II, whose data is described in this report, had a more closely defined set of goals, i.e.:

- 1. To compare the distribution of eddy statistics at 4000 m depth with similar results along 70°W,
- 2. To examine the vertical structure of the eddy field for qualitative differences in and out of the recirculation region of the western eddy of the North Atlantic subtropical gyre suggested by Worthington (1976),
- 3. To investigate the horizontal heat advection and local temporal changes of temperature,
- 4. To estimate some of the Reynolds stress contributions to momentum and vorticity budgets for the mean flow,
- 5. To examine energy transfer terms,
- 6. To compare the data obtained with the results of numerical models,
- 7. To compare the distribution of mean velocities obtained with the structure of the general circulation as suggested by Worthington (1976). Some of these results are described in Schmitz (1977).

Array II consisted of three nine-month mooring settings at twelve locations (Fig. 2) between May 1975 and June 1977. The third setting included moorings at three additional locations to better resolve, spatially, the subtropical gyre's return flow.

Array III consisted of three clusters. Clusters A and B were on the western and eastern sides of the Mid-Atlantic Ridge to examine differences in the eddy field and the mean flow. The purpose of cluster C was to look at the baroclinic instability of the North Equatorial Current, as an eddy-generating device.

Data from POLYMODE Array II are described in this report. Data from Arrays I and III will be presented in future reports.

Moorings

The POLYMODE Array II mooring configuration is shown in Figure 2. Moorings 1 through 12 were in position from May 1975 to June 1977 with three consecutive settings of approximately nine months duration. Mooring positions 13, 14 and 15 were deployed on the third setting of the array only (See Table 1).

Moorings 1 through 8, 13, and 14, were intermediate moorings (Heinmiller, 1976), moorings 9 through 12 and 15 were bottom moorings.

A complete list of the components of each mooring is shown on microfiche, in Row A. The following abbreviations have been used:

VACM	Vector Averaging Current Meter
DT-VACM	A VACM which also measures differential temperature
850	Model 850 burst sampling current meter
T/P	M.I.T. temperature and pressure recorder
3/4";5/8";3/4"	For example; $3/4$ " line used on set 1 and 3,
	5/8" line used on set 2
3/8" chain	Refers to the indicated length of 3/8" chain
	bolted to a 16" or 17" glass sphere in a hard
	hat (for flotation)

Array 2 was set as follows:

Ship & Cruise #	Mission		Chief Scientist(s)	Date
KNORR 49	Deployed Set 1	G.	Tupper/Dr. W. Schmitz	May 1975
CHAIN 129	Recovered Set 1		K. Bradley	December 1975
	Deployed Set 2			
KNORR 60	Recovered Set 2	к.	Bradley/D. Simoneau	October 1976
	Deployed Set 3			
KNORR 66	Recovered Set 3	к.	Bradley/D. Simoneau	June 1977

Current Meter Types

The current meters described in this report were either Vector Averaging Current Meters (VACMs), built by American Machine and Foundry (AMF) or Model 850 current meters built by Geodyne, now a part of Egerton, Germeshausen and Grier (EG&G).

The VACM senses compass and vane information and computes a measure of east and north water current components each time a pair of rotor magnets passes the sensing diode, then sums these components through the entire recording interval, usually 15 minutes. There are 16 magnets on the rotor so one complete rotor revolution would cause eight compute cycles.

Temperature is derived from a voltage-to-frequency converter (v/f), whose output frequency is related to the thermistor resistance at its input. The v/f output pulses are summed over the entire recording interval thus averaging temperature. All variables are recorded on a cassette tape at the end of each recording interval. Temperatures are accurate to about $\pm .01$ °C (Payne et al., 1976).

Temperature/Pressure Recorder

An instrument to record temperature, pressure and time (T/P) was developed in the Draper Laboratory at M.I.T. for MODE-1 and used extensively on the post-MODE moorings. The instrument stores a sample every 15 seconds and records the sum of 64 successive data samples every 16 minutes on a magnetic tape cassette $(64 \times 15 = 960 \text{ seconds} = 16 \text{ minutes})$.

Temperatures have a resolution of .001°C (Wunsch and Dahlen, 1974). The absolute accuracy cannot be specified because the thermistors had not been calibrated since the original calibration by the manufacturer.

The pressure sensor is a strain gauge with a manufacturer specified accuracy of .03% of the scale range used (Wunsch and Dahlen, 1974).

These sensors are recalibrated for each instrument deployment.

Occasionally the T/P sensors reached the limit of their measuring range. For instance, page/fiche no. 1-E-9.

A device to measure conductivity, temperature and pressure, manufactured by Neil Brown Instrument Systems, Inc. (N. Brown, 1975), was used at POLYMODE mooring sites to obtain vertical profiles of these quantities. Plots of temperature and salinity versus pressure, and θ -S plots are included for most POLYMODE mooring sites. The data were

collected on R. V. CHAIN cruise 129 and R. V. KNORR cruise 60. The plots are presented in Row A fiche 2-5 after the mooring page except for POLYMODE moorings 9, 10, 11, and 12 which are on fiche 5 columns 13 and 14.

Time

Time from T/Ps, 850s and VACMs was measured using a quartz crystal oscillator with a manufacturer's specified accuracy of ±1 second per day. In this report time is read as year-month-day hour.minute.second.

Current Meter Data Processing

Bit strings from magnetic sea tapes for Model 850s (1/4" 2-track cartridges) and VACMs (1/8" 4-track cassettes) were transcribed onto 9-track computer compatible tape at W.H.O.I. The data were then converted to scientific units (decoded) and stored on magnetic tape in Maltais format (Maltais, 1969)

Editing the data included selecting start and stop times, adjusting the nominal depth of some records to agree with information supplied by the T/Ps, applying corrections to temperature indicated by post cruise thermistor calibrations, correcting the temperatures to a constant depth, computing vector averaged components for the data from burst sampled Model 850 instruments, and interpolating through gaps in the data caused by the removal of erroneous records.

The result is an evenly spaced time series which is used as input for the low pass filter, a symmetrical running Gaussian filter with a half width of 24 hours and a window of width 24 hours. The filtering is sequential and the resultant time series is 48 hours shorter than the input time series (the first and last 24 hours are lost).

There is usually a three or four day gap between data series from consecutive settings. On some composite plots the gap is shown. On others, such as spectra and spatial array plots, the gap has been filled with interpolated points.

Table 2 indicates which variables are presented, with reference to data identification number, duration and depth.

Data Identifiers

To insure that each data series has a unique identifier, the tollowing scheme is used; 6081B1DG24A.

- The first three digits are the mooring number.

The relative instrument position starting at the top of the mooring. One denotes the top instrument.

B - The position of the letter in the alphabet indicates the amount of editing that has been done. The symbol \$ means no editing has been done.

1DGau24 } - A 1-day subsampled Gaussian filtered series, the filter having a half width of 24 hours.

 Additional editing has been done after the series was filtered.

As the time series from the 3 settings have been merged together, additional naming parameters have been used; PMO2,4000m.

PM - POLYMODE Array II

02 - POLYMODE mooring position number 2.

- A separator.

4000 m - The nominal depth in meters for the merged data series.
or
4 km

Current meter data quality

Overall, the data return from the three settings was about 90%. A total of 133 current meters was set. One hundred had 100% data return, eight returned no data, and twenty-five had less than 100% return.

An unsolved problem affected several of these twenty-five. The symptom is a sudden drop in speed to threshold or near threshold followed by another sudden jump back to normal values. The low values usually persist for a few hours to a few days. Total data loss from this problem is 19 days in five records. In these periods speeds have been replaced by interpolated or averaged values. Much testing and speculating have not yet determined the cause of the problem. Occurrences are noted on the STATISTICS pages in the microfiche section. Other problems also are noted on these pages. For example, "sticky vane" indicates that the high frequency data may not be reliable during specified periods. For the most part this did not seriously affect the low-passed version. Where it did, the data have been deleted.

pepth

A summary of all instrument depths is presented in Table 2. Three depth designations have been used. First is a design or nominal depth, which was proposed for the experiment, and which is used in titles and composite displays. Second is an instrument depth which was computed after mooring deployment by buoy computer program NOYFB, and which is used on the mooring component pages and for records from current meters set deeper than 1500 meters. Third is a corrected depth, whose derivation is described in a separate paragraph, and which is used when data for individual records are presented.

POLYMODE Array 2 Temperature and Depth Corrections

Because of the occasional high currents seen by this array and the resulting depth variations of the moorings (up to hundreds of meters) it was desirable to attempt to correct to a constant depth the temperatures from both T/Ps and current meters. To make this correction it was necessary to know both the depth of an individual instrument and the temperature structure in the water above it. Pressures from T/Ps were used to compute depths for these instruments. Current meter depths were interpolated from them.

Figure 4 is a plot of temperature gradient $\frac{dT}{dp}$ vs. absolute temperature T. The data are from CTDs taken at the time of deployment and recovery of each mooring and represent stations from the full north-south extent of the array. The most northerly stations were in the Gulf Stream. It is apparent that one can represent quite simply the relationship between $\frac{dT}{dp}$ and T for the whole Array 2 area. The two straight lines on Fig. 4 represent a least squares fit of the data and were used in the temperature correction.

The following procedure was performed on the 1DGAU24 version of each instrument record with a depth of 1500 m or shallower ($\frac{dT}{dp}$ is negligible at greater depth). For each file:

 Create PDIF for each T/P record by subtracting the most frequent pressure in the record from each pressure value in the time series.

- 2. Create PDIF for each current meter record. This may be:
 - a. The same as the PDIF for a T/P if there is one quite near on the mooring.
 - b. An average of the PDIFs from nearby T/Ps if the current meter is between two of them.
 - c. For a current meter deep on a mooring which has T/Ps only near the top, PDIF is PDIF for one of the shallow T/Ps multiplied by an attenuation factor.

For each data point:

- 3. Compute dT/dp at the observed temperature.
- 4. Compute a corrected temperature using PDIF and dT/dp.
- 5. Determine dT/dp at the corrected temperature.
- Recompute the corrected temperature using PDIF and the mean of the two dT/dps.
- 7a. For T/P records, compute a depth for each pressure by multiplying the pressure by a factor determined by converting the most frequent pressure of the record to a depth, using the method of Saunders and Fofonoff (1976).
- 7b. For current meter records, compute a depth for each data cycle by adding to the most frequent depth of the record (obtained by interpolation of T/P values on that mooring) the value of PDIF (including attenuation factor) used for correcting the temperature of that data cycle multiplied by a conversion factor obtained from Saunders and Fofonoff (1976) for the depth and geographical position of the current meter.

One of the results is a most frequent depth for each record. These depths are shown as a corrected depth for each record in Table 2.

The basic statistics and plots on the fiche pages show values for uncorrected temperature. The spectra (on the fiche) and the composite plots following the text use corrected temperature.

Programs

Statistics (STATS)

We have presented some different statistical parameters in this report to reflect changes in the techniques being used to analyze our current meter data.

Means of the east (u) and north (v) components of velocity are, to some extent, misleading since orienting the reference frame to the compass may not shed any light on the physics of the problem. In some cases, however, we can choose a reference frame which may have a particular meaning. If we rotate the reference frame by θ , then we can transform the fluctuating parts of the u and v velocity components into

$$u' = u \cos\theta + v \sin\theta$$

 $v' = -u \sin\theta + v \cos\theta$

The time average of the squares of the individual components and their product are given by

$$\overline{\mathbf{u}^2} = \frac{\overline{\mathbf{u}^2 + \overline{\mathbf{v}^2}}}{2} + \frac{\overline{\mathbf{u}^2 - \overline{\mathbf{v}^2}}}{2} \cos 2\theta + \overline{\mathbf{u}^2} \sin 2\theta$$

$$\overline{\mathbf{v}^2} = \frac{\overline{\mathbf{u}^2 + \overline{\mathbf{v}^2}}}{2} - \frac{\overline{\mathbf{u}^2 - \overline{\mathbf{v}^2}}}{2} \cos 2\theta + \overline{\mathbf{u}^2} \sin 2\theta$$

$$\overline{\mathbf{u}^2 \mathbf{v}^2} = \overline{\mathbf{u}^2 \cos 2\theta} - (\frac{\overline{\mathbf{u}^2 - \overline{\mathbf{v}^2}}}{2}) \sin 2\theta.$$

Now $\overrightarrow{u} \overrightarrow{v}$ is the correlation between the two components and, by choosing θ properly we can cause $\overrightarrow{u} \overrightarrow{v} = 0$. This value is

$$\tan 2\theta_{N} = \frac{\overline{uv}}{\frac{1}{2}(\overline{u^2} - \overline{v^2})}.$$

At θ_N , then, the u and v motions are either totally uncorrelated in the mean, or they have a constant phase difference of 90°. If they have a constant phase difference then we can describe the motion of the velocity vector in u-v space as elliptical.

It is convenient to define two quantities invariant under rotations of the coordinate axes:

$$E = \frac{1}{2} (\overline{u^2} + \overline{v^2})$$

$$R^2 = (\overline{uv})^2 + \frac{1}{2} (\overline{u^2} - \overline{v^2})$$

where E is our normal definition of horizontal kinetic energy.

It is convenient and consistent with our definitions of R and θ_{N} to set

$$\overline{uv} = R \sin 2\theta_{N}$$

$$\frac{\overline{u^2} - \overline{v^2}}{2} = R \cos 2\theta_{N}$$

And, for arbitrary θ ,

$$\overline{\mathbf{u}^2} = \mathbf{E} + \mathbf{R} \cos 2(\theta_{\mathbf{N}} - \theta)$$

$$\overline{\mathbf{v}^{2}} = \mathbf{E} - \mathbf{R} \cos 2(\theta_{\mathbf{N}} - \theta)$$

$$\overline{\mathbf{u}'\mathbf{v}'} = R \sin 2(\theta_{\mathbf{N}} - \theta)$$

For
$$\theta = \theta_{N}$$
,

$$\overline{u^2} = E + R$$

$$\overline{v^2} = E - R$$

$$\vec{\mathbf{u}} \cdot \vec{\mathbf{v}} = 0$$

If we view the path of the velocity vector as elliptical in $\,u\text{-}v\,$ space then $\sqrt{\,u^{\,2}\,}\,$ and $\sqrt{\,v^{\,2}\,}\,$ are the major and minor axes and $\,\theta_{\,n}\,$ is the orientation of the major axis .

In order to know if it makes sense to talk about principal axes we need one more index, ellipticity, defined by

$$\mathbf{e} = \frac{\sqrt{\overline{\mathbf{u}^2}} - \sqrt{\overline{\mathbf{v}^2}}}{\sqrt{\overline{\mathbf{u}^2}}}.$$

Ellipticity varies from 0 for circular motion, in which case it makes no sense to talk about principal axes, to 1 for motion strictly along the major axis.

This definition of ellipticity is for means over the full record length. For rotary quantities in most records it is more interesting to look at the variation of ellipticity with time. Dividing the record into pieces, computing the ellipticity for each piece and then averaging these ellipticities generally gives a larger mean.

Progressive Vector Diagram (PROVEC)

The progressive vector displacements are plotted. These are derived by multiplying the average speed in an interval by the interval length and joining the resulting vectors head-to-tail. The plot begins with an asterisk (*). All following month boundaries are indicated by the symbol \bigcirc .

Variable vs. Time Plot

This is a diagram of any variable plotted as a function of time.

The 24 hour averaged components are plotted as individual vectors along a time scale. Unless otherwise indicated, the vector orientation is such that east is up.

Sequential Array Plots

Subsampled filtered velocity vectors or temperature values are plotted to show a spatial array at a particular depth.

Spectra

The program TIMSAN (<u>Time Series Analysis</u>) uses the Fast Fourier Transform algorithm of Singleton (1969) and is restricted to data segments of length N points, where N must be an even number which has no prime factor larger than 5, and must be less than 8000 points.

The number of degrees of freedom for the first 40 plotted points is given by V = a m s where m is the number of adjacent frequency bands being averaged, s is the number of independent data pieces being averaged, again as stated in the label, and a is 2 for temperature spectra and for Horizontal Kinetic Energy (HKE) spectra for which the EAST and NORTH components seem statistically independent. In the absence of information regarding NORTH-EAST correlation, one should use a = 2 to be safe.

The log-log plot is further averaged during plotting so that more and more points are averaged together as frequency increases. This eliminates the bunching together of points at high frequencies, increases the degrees of freedom of the high frequency estimates, and still permits low-frequency resolution.

Averaging is as follows:

Plotting Pts.	Frequency Bands Averaged Over	Data Points	Cumulative Data Points	Degrees Freedom
First 40	5	200	200	10
Next 15	10	150	350	20
Next 6	25	150	500	50
Next 6	50	300	800	100

In this way, for example, 750 data points would be plotted as only 66 points. The m in the formula v = a m s for degrees of freedom is, in this example, 10 times larger at the highest frequencies than at the lowest frequencies.

For $v \ge 30$, the confidence limits for the spectral estimates are given approximately by $(1-2/9v \pm 2\sqrt{2/9v})^{\frac{1}{3}}$ where Z=1.28375 for 80% confidence limits, Z=1.645 for 90%, Z=1.96 for 97% and Z=2.5757 for 99%. In the example above, if the HKE spectral plot label had indicated 2 pieces and averaging over 8 adjacent frequency bands then $v=2\times 2\times 8=32$ for the lowest frequencies (assuming NORTH and EAST components are highly correlated) and $200\times 32=6400$ for the highest frequencies. The 95% confidence intervals (i.e., 95% of the time one would expect the spectral estimates to vary no more than this much) would be (0.57, 1.55) at low frequencies, and (0.97, 1.03) at high—frequencies.

For $\nu \leq 30$, one must obtain confidence intervals from Chi-Squared distribution tables in standard statistical references.

Float Tracks

Free drifting buoys have been deployed several times in the North Atlantic since 1977 as part of a study of the Gulf Stream System (Richardson, 1977).

The buoys had a 200 m line-drogue and a temperature sensor, and were tracked by the Nimbus F satellite. The buoy tracks shown in Fig. 3 are a few of those measured during the time of the Array 2 experiment.

References

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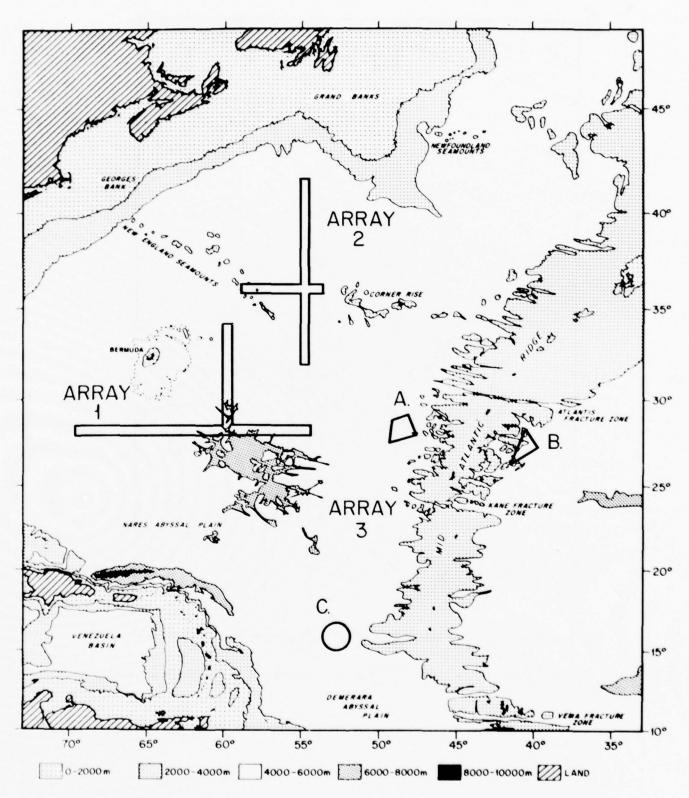


Figure 1. Location of POLYMODE Arrays 1, 2 and 3

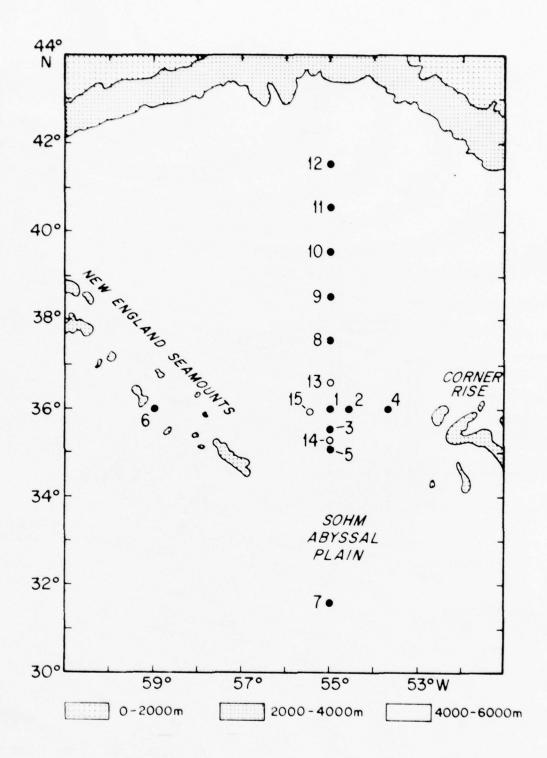


Figure 2. Location of moorings, Array 2

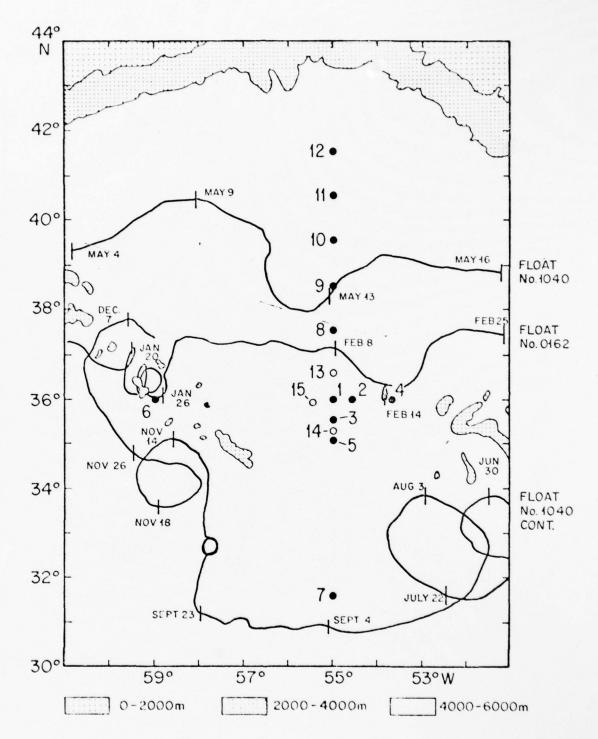


Figure 3. Float tracks, 1977

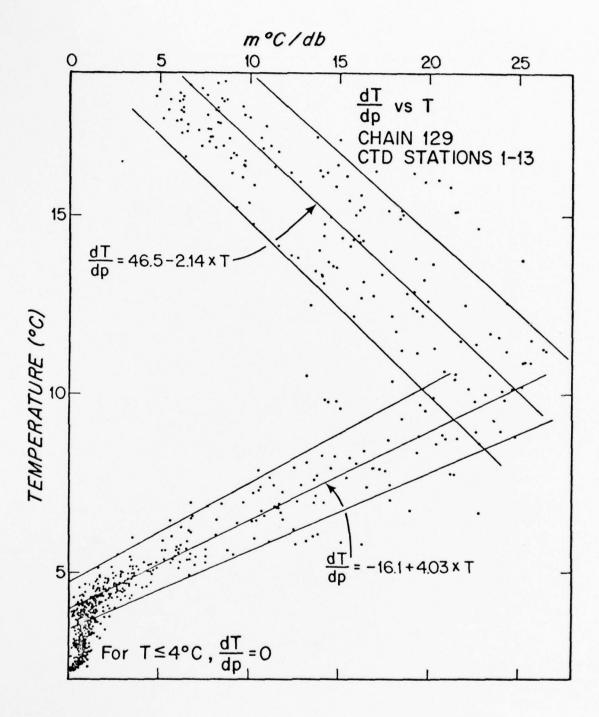


Figure 4. Depth correction curve

Table 1
MOORING NUMBERS, LOCATIONS AND DURATION

POLYMODE #		PM01			PMO2			PM03			PMO4	
W.H.O.I. #	557	583	608	558	579	600	565	582	609	F 559	578	601
LOCATION (°N)	35°56' 55°06'	35°53' 55°03'	35°53' 55°05'	35°57° 54°41°	35°56' 54°52'	35°55' 54°44'	35°36' 55°05'	35°36' 55°05'	35°36' 55°05'	35°58' 53°46'	35°58' 53°45'	35°58' 53°47'
SET DATE	May 3 75	Dec 18 75	0ct 15 76	May 4 75	Dec 12 75	Oct 4 76	May 8 75	Dec 18 75	0ct 15 76	May 4 75	Dec 11 75	Oct 5 76
RETRIEVAL DATE	Dec 18 75	Oct 14 76	July 3 77	Dec 12 75	Oct 4 76	May 29 77	Dec 18 75	Oct 15 76	July 3 77	Dec 11 75	Oct 5 76	May 30 77
BOTTOM DEPTH (meters)	5089	5043	5054	5379	5338	5318	5162	5107	5115	5478	5463	5467
POLYMODE #		PM05			PM06			PM07			PM08	
W.H.O.I. #	566	581	611	568	584	598	567	580	612	564	577	606
LOCATION (°N)	34°53' 55°02'	34°56' 55°05'	34°56' 55°05'	35°56' 59°02'	35°57' 59°02'	35°55' 59°02'	31°36' 55°05'	31°35' 54°56'	31°35' 54°56'	37°30' 55°00'	37°29' 55°01'	37°29' 55°00'
SET DATE	May 9 75	Dec 17 75	Oct 17 76	May 15 75	Dec 20 75	Oct 2 76	May 14 75	Dec 15 75	Oct 19 76	May 7 75	Dec 10 75	Oct 12 76
RETRIEVAL DATE	Dec 17 75	Oct 17 76	July 2 77	Dec 19 75	0ct 2 76	May 28 77	Dec 15 75	Oct 19 76	June 21 77	Dec 10 75	Oct 12 76	July 5 77
BOTTOM DEPTH (meters)	5515	5502	5506	5205	5202	5206	5296	5587	5595	5350	5310	5334
POLYMODE #		PM09			PM10			PM11			PM12	
W.H.O.I. #	563	576	605	562	575	604	561	574	603	560	573	602
LOCATION (°N)	38°30' 54°58'	38°30' 54°55'	38°29' 54°56'	39°27' 54°59'	39°30' 55°00'	39°29' 55°01'	40°28' 55°00'	40°27' 55°03'	40°27° 55°03°	41°29' 55°00'	41°29' 54°59'	41°29' 54°58'
SET DATE	May 7 75	Dec 9 75	Oct 11 76	May 7 75	Dec 8 75	Oct 10 76	May 6 75	Dec 8 75	Oct 9 76	May 6 75	Dec 7 75	Oct 8 76
RETRIEVAL DATE	Dec 9 75	Oct 10 76	July 5 77	Dec 8 75	Oct 10 76	July 7 77	Dec 8 75	Oct 9 76	July 8 77	Dec 6 75	Oct 7 76	July 9 77
BOTTOM DEPTH (meters)	5353	5340	5340	5279	5264	5266	5171	5177	5173	4774	4758	4772
POLYMODE #				PM1 3	PM14	PM15						
W.H.O.I. #				607	610	599						
LOCATION (°N)				36°30' 55°00'	35°15' 55°00'	35°57' 55°28'						
SET DATE				0ct 13 76	0ct 16 76	Oct 3 76						
RETRIEVAL, DATE				July 4 77	July 3 77	May 29 77						
BOTTOM DEPTH (meters)				5445	5487	5457						

Table 2

a. Data Variables, Moorings 1-5

Inst.	Nominal	Data			Ve.	locit	cies		Temp	erati	ire		Pr	essu	ire	
Туре	Depth	Ident.		1		+	+)			+][+	+	
	(m.)	no.	S	et	1	2	3	_/	1	2	3	1	1	2		3
POLY!	MODE moo	ring positio	n #1	W.H	.0.	T. mc	ori	nas	#557,	#58	3. #	608				
CM.	600	1;1;1		<u></u>		-	+	-				-11		+	+	
r/P	800	2;2;2		1		+	+	i	-			-1 [
CM	1000	3;3;3				· 	<u>.</u>					1 [+	+	
r/P	1200	4;4;4		1		+	+	1	<u></u>			1 6		<u>.</u>		
CM	1500	5;5;5		- 1					[,			1 [,	
r/P	2000	6;6;6		ı		-	+	1	<u> </u>		+] [1		
r/P	2500	7;7;7		ſ		+	+	1					_		-	
				1								٦ -		-	-	
T/P	3000	8;8;8		1		+	+ +]] [_	
T/P	3500	9;9;9		l ,			+	1				٦.			+	
CM	4000	10;10;10					7	i][+	+	
T/P	4500	11;11;11		l		+	+	1	-			7		+	+	
T/P	5000	12;12;		- E		+	+]	-		+	11		+	-	
CM	5000	; ;12		i		۲	-	-	l +			11		+	+	
*POLY	MODE moo	ring position	n #2	W.H	.0.	I. Mo	ori	ngs	#558,	#579	9, #6	600				
CM	600	1;1;1		[+	-	[+			-][+	+	
Incl	800	2; ;		[+	+]	[+		+][+	+	
T/P	800	3;2;2		[+	+]				4		+	+	
CM	1000	4;3;3		-			+		+][+	+	
CM	1500	5;4;4		-			+	-	-+] [+	+	
Incl	1500	6; ;		1		+	+	1	[+		+][+	+	
Inc1	3000	7; ;		1		+	+]	+]		+	1[+	+	
r/P	3000	8;5;5		1		+	+	1				-1 1-		+	-+	
CM	4000	9;6;6		-			+		+			-11		+	+	
Incl	4000	10; ;		1		+	+]	1 +		+	1[+	+	
r/P	5000	11;7;7		[+	+]				11		+	+	
*POLVI	MODE moo	ring position	n #3	TAT I-I	0	T Mc	ori	nae	#565,	#50) #6	sna				
CM	600	1;1;1	11 113	W - 11		L. PIC	- T	195	H 303,	#50.	-, "	-1 [+	+	
r/P	800	2;2;2		1		-	+	1				71			+	
CM	1000	3;3;3		1			+					41		+	+	
CM	1500	4;4;4					-					-) I		+	+	
r/P	3000	5;5;5				-	+	1				71			+	
				1				1				7 [
CM	4000	6;6;6		-			-		·			-] [+	+	
IES	5000	; ;7		1		+	+	1][+	+	
CM	5000	; ;8		l		+	+	-		-		1		+	+	
r/P	5000	7;7;9		1		+	+]						+	+	
POLY	MODE moo	ring position	n #4	W.H	.0.	I. Mo	ori	ngs	#559,	#578	3, #6	501				
CM	600	1;1;1		-		-	+	-				1+		+	+	
r/P	800	2;2;2		[-	+	+	1			-	11		+	- +	
M	1000	3;3;3		1			+	-	1 +			i		+	+	
M	1500	4;4;4		-			-	-				-11		+	+	
CM	4000	5;5;5		-			+	<u></u>	-+			-i i		+	+	
	MODE: mass	ring position	n #6	Va7 . 1.1	0 .	. M-	ori-		#566,	#50		211				
POLYF CM	600	1;1;1	U #3	W.H	.0.	. MC	Orn	195		#38.	, #	11		+	+	
r/P	800	2;2;2		1		-	+	1				11			,	
CM	1000	3;3;3		-								11		+	+	
CM CM	1500	4;4;4		1				1				11		+	+	
	1 7(1)	(4:4:4		-												

Table 2
b. Data Duration and Depths, Moorings 1-5

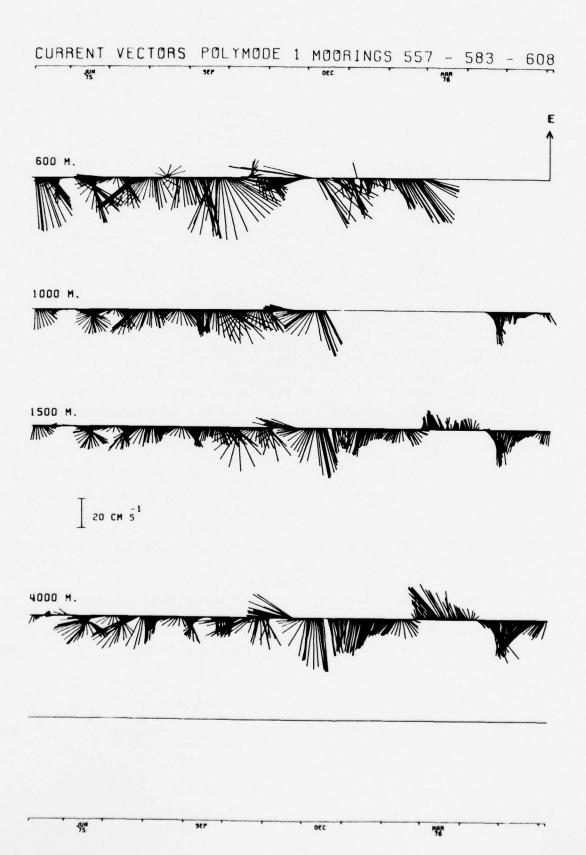
			Depths					Data D			Dat	a Iden	t.
Set	1	2	3	1		Set	1	2	3			No.	
*POI	YMODE	moor	ing pos	ition	#1			W.1	1.O.I.	Moorings	#557,	#583,	#608
	603	614	595				224	74	259		1;	1;	1
	802	815	795				224	298	260		2;	2;	2
	1004	1017	1001				224	180	259		3;	3;	3
	1204	1219					224	298	0		4;	4;	4
	1503	1501	1503				226	298	259		5;	5;	5
	2002	2006	2003				53	291	260		6;	6;	6
	2505		2501				224	0	260		7;	7;	7
	3001	3011					224	298	O		8;	8;	8
	3501		3500				225	0	260		9;	9;	9
	4001	4001					224	298	0		10;	10;	10
	4495	4506	4502				224	298	260		11;	11;	11
		5011					0	298	-		12;	12;	
			5003				-	-	259		;	;	12
POI	YMODE		ing pos	ition	#2			W.H	.0.1.	Moorings	#558,	#579,	#600
		563	596				0	292	235		1;	1;	1
											2;	;	
	781	758	796				213	215	235		3;	2;	2
	982	966	996				215	294	235		4;	3;	3
	1482	1468	1498				215	294	235		5;	4;	4
											6;	;	
											7;	;	
	2992	2959	3001				219	294	235		8;	5;	5
	3977	3955	4002				218	294	235		9;	6;	6
											10;	;	
	4964	4944	5006				218	294	235		11;	7;	7
POL	YMODE	moori	ng pos	ition	#3			W.H	.O.I.	Moorings	#565,	#582,	#609
	640	698	720				219	300	257		1;	1;	1
	840						219	0	0		2;	2;	2
	1040		1120				219	O	257		3;	3;	3
	1540	1605	1620				219	284	257		4;	4;	4
	3035	3108	3117				220	300	258		5;	5;	5
	4030	4106	4000				219	300	257		6;	6;	6
											;	;	7
			5128				-	-	255		;	;	8
	5021	5095	5129				219	300	258		7;	7;	9
POL			ng pos		#4			W.H	.o.I.	Moorings	#559,	#578,	#601
	601	588	603				217	246	234		1;	1;	1
	802	790					217	246	0		2;	2;	2
		991	1003				0	246	234		3;	3;	3
	1501	1494	1503				217	246 2	214/23	4	4;	4;	4
	4001	3996	4003				177	246	234		5;	5;	5
POL			ng pos	ition	#5			W.H	.o.I.	Moorings	#566,	#581,	#611
	606	633	596				219	301	204		1;	1;	1
	807	835	796				219	301	204		2;	2;	2
	1006	1036	996				219	301	204		3;	3;	3
		1540	1498				219	71/301	204		4;	4;	4
	4006	4041					219	301	0		5;	5;	5

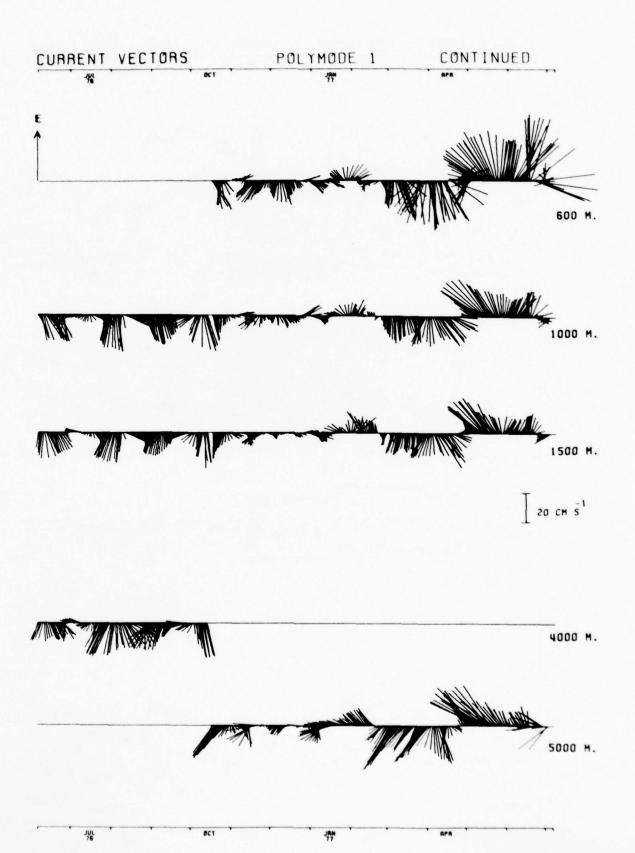
Table 2
c. Data Variables, Moorings 6-15

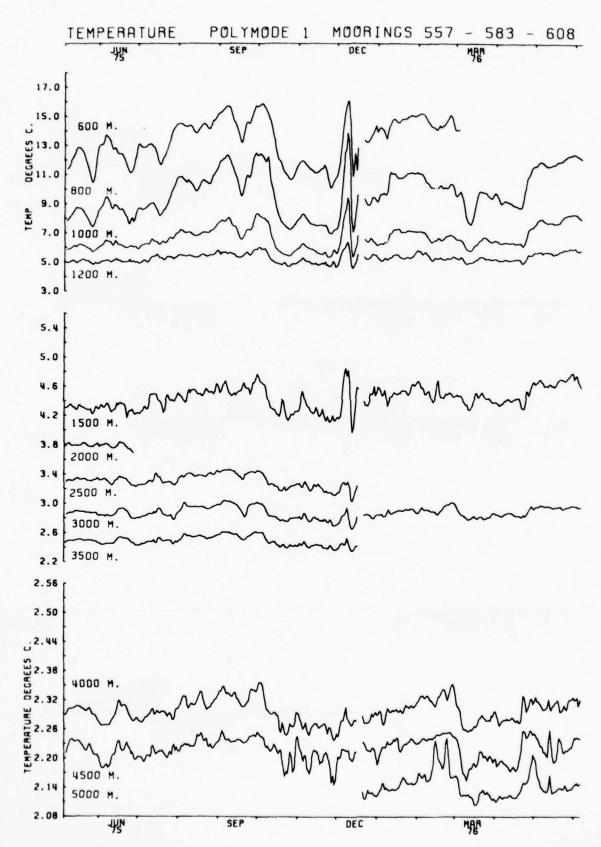
Inst.	Nominal	Data		Ve	eloc	ities	Temp	peratu	ire	Pre	essur	e
Тури	Depth	Ident.		[+	+][-	+ +	- 11	+		+]
	(m.)	no.	S	et 1	2	3	/ 1	2	3 /	1	2	3
*POLY	MODE MOOF	ing position	#6	W.H.O.	Ι. 1	mooring	s #568.	#584	. #598			
CM	600	1;1;1			+		1			+		+ 1
T/P	800	2;2;2		í	+	+	1	-	i E			+ 1
CM	1000	3;3;3		-	-		4		· ·	+		+ 1
CM	1500	4;4;4		-	-		4	-		+		+ 1
CM	4000	5;5;5		-	+	-	-i	-	1	+		+ 1
								11500				
		ing position	# /	W.H.O.	1. 1	mooring +	s #567,					. ,
CM	600 800	1;1;1		[-] [- +	, ,	+		+]
CM		; ;2		ſ	+			+ +	, ,	+		+]
T/P	800 950	2;2;3		l l	++	+] [
CM		; ;4		l			-} [+		[+		+]
CM	1000	3;3;5		[-		1 [[+		+]
CM	1500	4;4;6					1 [-		[+		+]
CM	2000	; ;7		1	+] [+		[+		+]
CM	2500	; ;8		l	+	+	-][+	+	[+		+]
CM	4000	5;5;9			+		7	-	 1[+		+]
* POLY		ing position	#8	W.H.O.	I. 1	mooring	s #564,	#577	, #606			
CM	600	1;1;3		{	+		4	+	[+		+]
T/P	800	2;2;2		[+	+] [+		+]
CM	1000	3;3;		-	+		} [+][+		+]
CM	1500	4;4;4		-	+		1		 [+		+]
CM	4000	5;5;5		-	+	-+	1	++	 [+		+]
*POLY	MODE moor	ing position	#9	W.H.O.	T. 1	mooring	s #563,	#576	. #605			
CM	4000	1;1;1	., -	-	+				1	+		+ 1
T/P	4000	2;2;2		1	+	+	11 +	,	- i -			1
CM	5250	; ;3		í	+	+	4 1			+		+ 1
T/P	5250	; ;4		ī	+	+	11 +			+		
		ing position	#10	W.H.C).1.	moorin	gs #562	2, #5/				
CM	4000	1;1;1		-	-		1		[+		+]
T/P	4200	2;2;2		1	+	+] [
*POLY!	MODE moor	ing position	#11	W.H.C).I.	moorin	gs #561	, #57	4, #603	3		
CM	4000	1;1;1		-	+-	-+			 [+		+]
T/P	4200	2;2;2		[+	+] [+		
*POLY!	MODE moor	ing position	#12	W.H.C).I.	moorin	gs #560	, #57	3, #602	2		
CM	4000	2;1;1		-	+	-+	1	+		+		+]
T/P	4000	1;2;2		1	+	+] [+		+		
*DOT V	MODE moor	ing position	#13	WHO) Т	moorin	ac		#607	,		
CM	600	; ;1	11.13	1	+][+			+		
CM	1000	; ;2		1	+] [+					. 1
CM	1500	; ;3		1	+	_	11 +					. 1
CM	4000	; ;4		1	+							. 1
												,
		ing position	#14	W.H.C		moorin			#610			
CM	600	; ;1		[+		+] (+		
CM	1000	; ;2		{	+		+ 1			+		+]
CM	1500	; ; 3		[+		+) [+		+ 1
CM	4000	; ;4		[+	+	4 1	+	[+		+ 1
*POLY	MODE moor	ing position	#15	W.H.C).I.	moorin	qs		#599)		
СМ	4000	; ;1		[+		- +	. +		+		+ 1
					137							

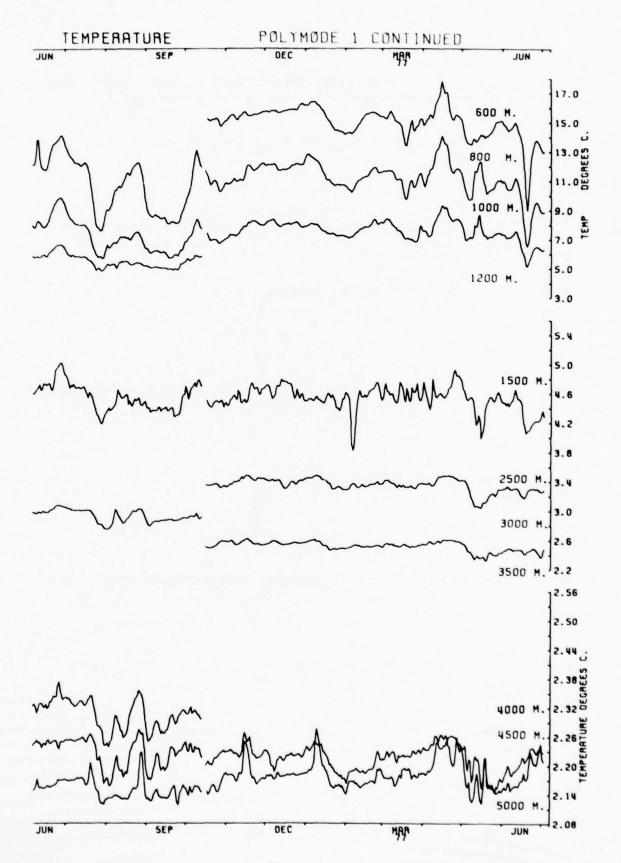
Table 2
d. Data Duration and Depths, Moorings 6-15

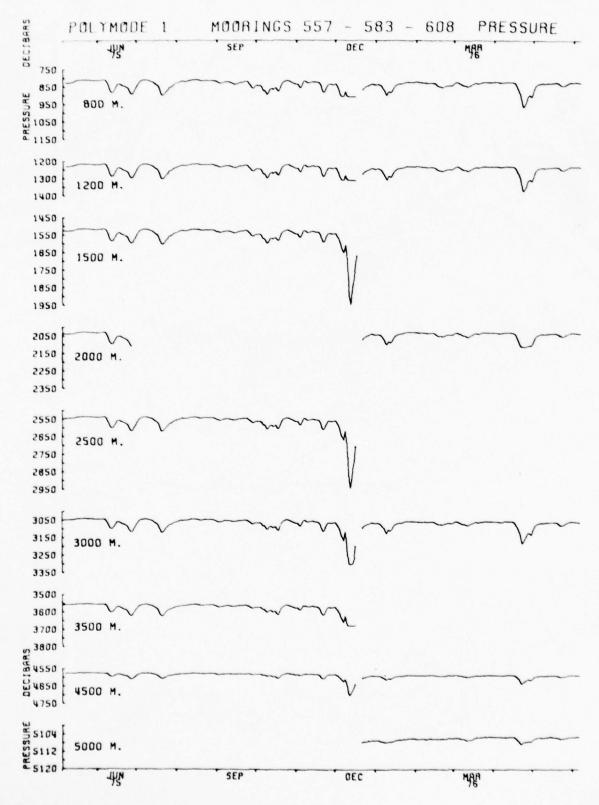
	Corr	ected	Depths (m)		# of	Data	Day	S		Dat	a Iden	t.
Set	1	2	3		Set 1	2	3				No.	
*PO	LYMODE	moori	ng position	#6		W.	н.о	.1.	Moorings	#568,	#584,	#598
	612		600		215	0		69		1;	1;	1
	813	814			215	28€	,	O		2;	2;	2
	1013	1015	1000		215	286/1	98	235		3;	3;	3
	1512	1518	1500		215	286		235		4;	4;	4
	4007	4019	4000		83	286		235		5;	5;	5
*POI	LYMODE	moori	ng position	#7		W.	н.о	.I.	Moorings	#567.	#580.	#612
	631	587	_		213	167		0		1;	1;	1
			763					243		;	;	2
	831	802	763		213	266		243		2;	2;	3
			913					243		;	;	4
	1031	990	965		213	306		243		3;	3;	5
	1531	1494	1470		37+120	304		243		4;	4;	6
			1976					243		;	;	7
			2483					243		;	;	8
	4031	3995	4003		213	306		243		5;	5;	9
*POI	YMODE	moori	ng position	#8		W	н О	т	Moorings	#564		4606
	627	583	585	110	212	304		263	root mgs			
	826	785	385		212	304		263		1;	1;	3
	1026	986	363		212			203		2;	2;	2
	1525	1490	1250			304		262		3;	3;	
	4014	3990	4013		212 212	304 304		263 263		4;	4;	4
					212	304		263		5;	5;	5
*bol			ng position	#9					Moorings	#563,	#576,	#605
	3990	3991	4035		212	304		265		1;	1;	1
	3991	3992	4044		212	304		166		2;	2;	2
			5246					265		;	;	3
			5247					265		;	;	4
*POI	YMODE	moori	ng position	#10		W.	н.о	Ι.	Moorings	#562,	#575.	#604
	3973	3990	4017		212	304		267		1;	1;	1
	4173	4190	4217		212	304		268		2;	2;	2
* POI	VMODE	moori	ng position	#11		W	н о	т	Moorings	#561		#602
	3970	3985	4039	11.1	211	303		269	MOOI THGS			
	4169	4185	4239		211	303		270		1; 2;	1;	1 2
+001												
POI			ng position	#12	211				Moorings			
	3948	3995	3982		211	302		272		2;	1;	1
	3946	3996	3983		211	303		272		1;	2;	2
*POI	YMODE	moorin	ng position	#13					Moorings			#607
			654				123,			;	;	1
			1054					261		;	;	2
			1553					261		;	;	3
			4049					261		;	;	4
*POI	YMODE	moorin	ng position	#14		W.	н.о.	Ι.	Moorings			#610
			596				2	257		;	;	1
			999				2	257		;	;	2
			1498				2	257		;	;	3
			3998				2	257		,	;	4
*POI	YMODE	moorin	ng position	#15		W.	н.о.	Ι.	Moorings			#599
			3997					235				1
										,		

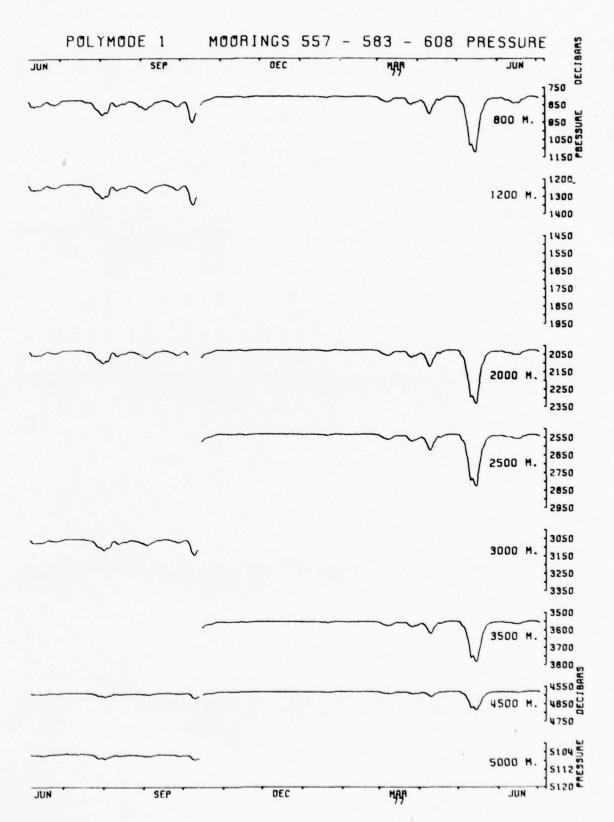








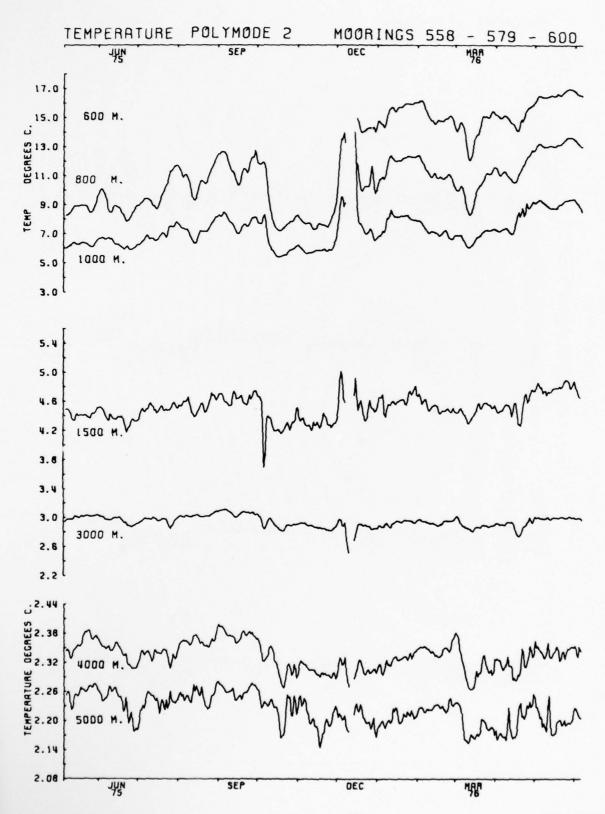


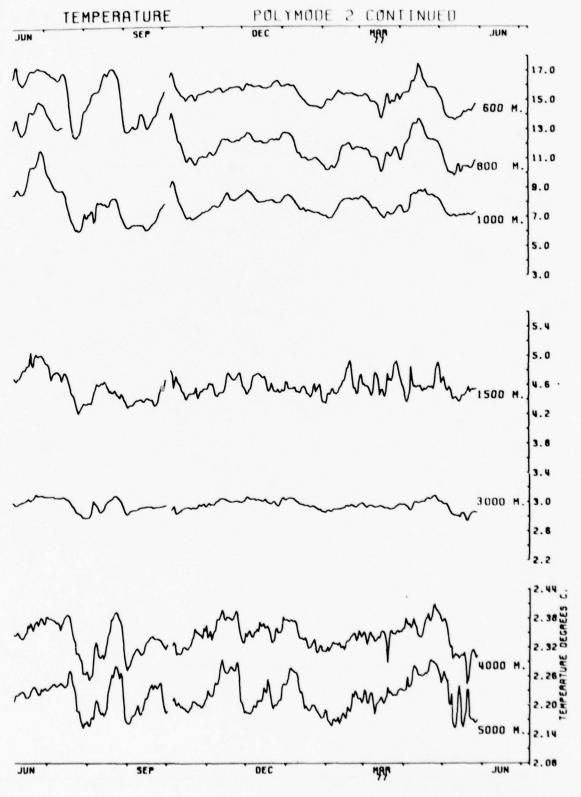


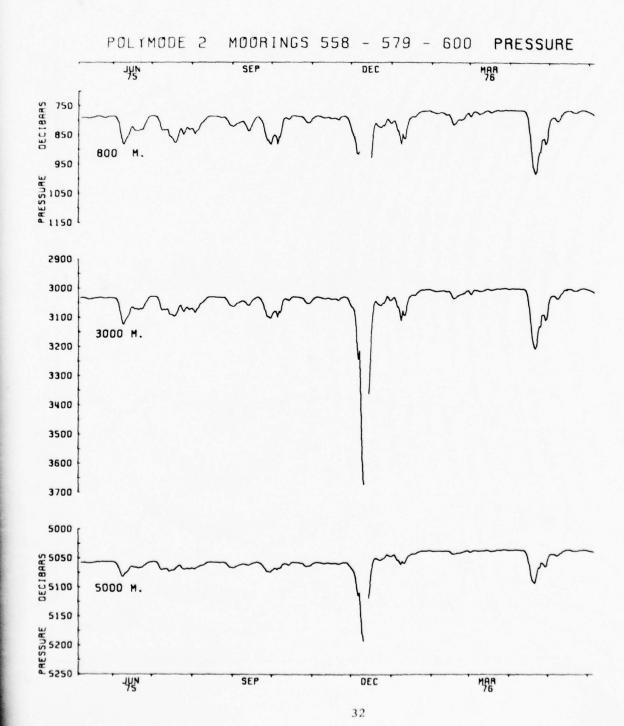
CURRENT VECTORS POLYMODE 2 MOORINGS 558 - 579 - 600 600 M. 1000 M. 20 CM 51 1500 M. 4000 M.

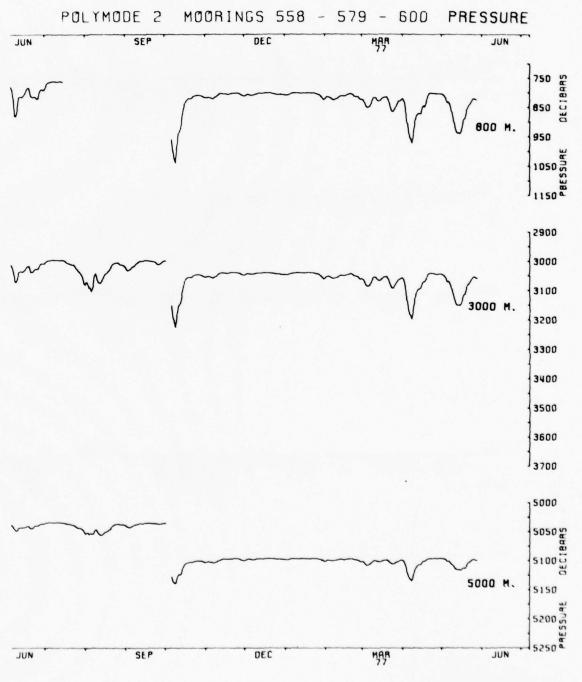
DEC

CURRENT VECTORS POLYMODE 2 CONTINUED 20 CM 51

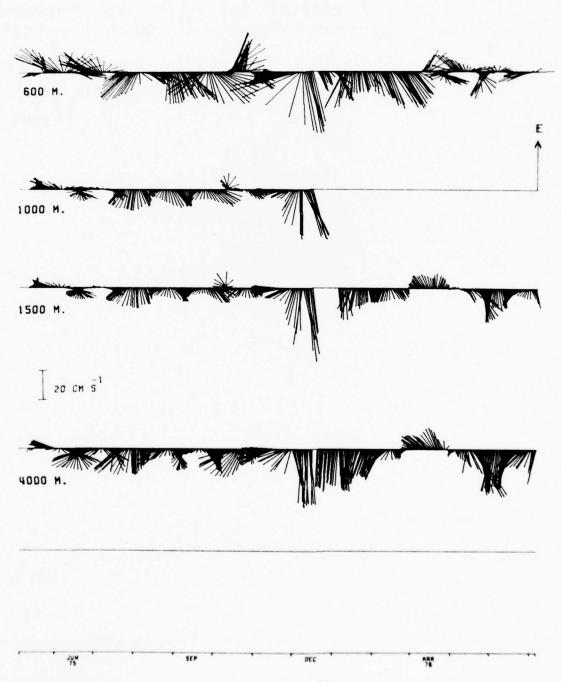






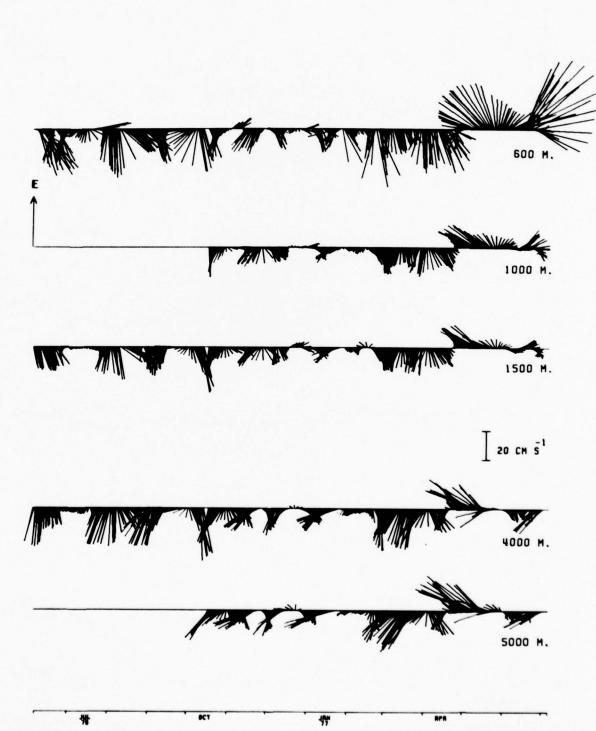


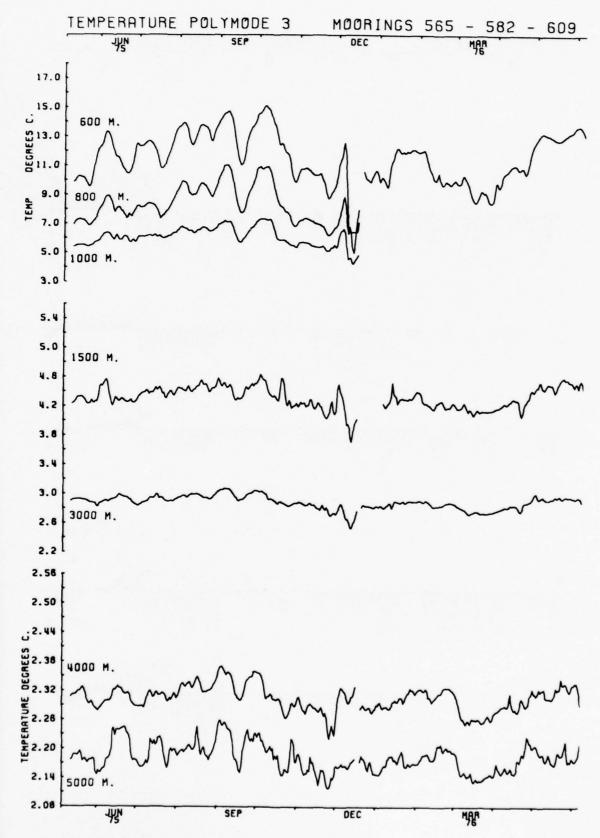
CURRENT VECTORS POLYMODE 3 MOORINGS 565 - 582 - 609

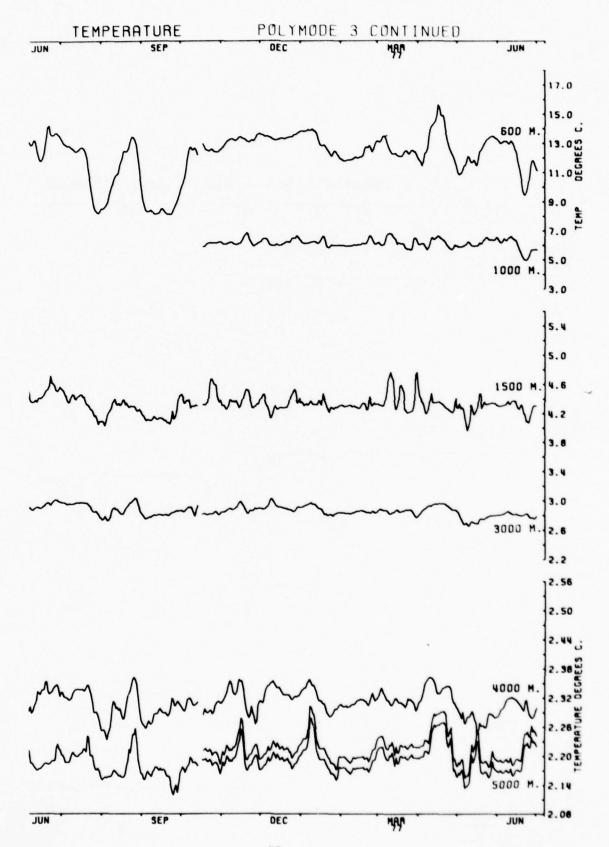


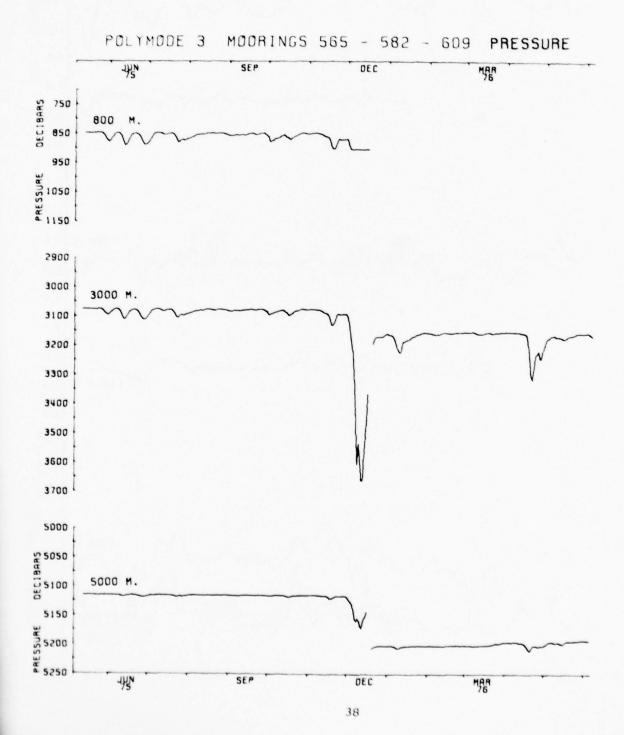
CURRENT VECTORS

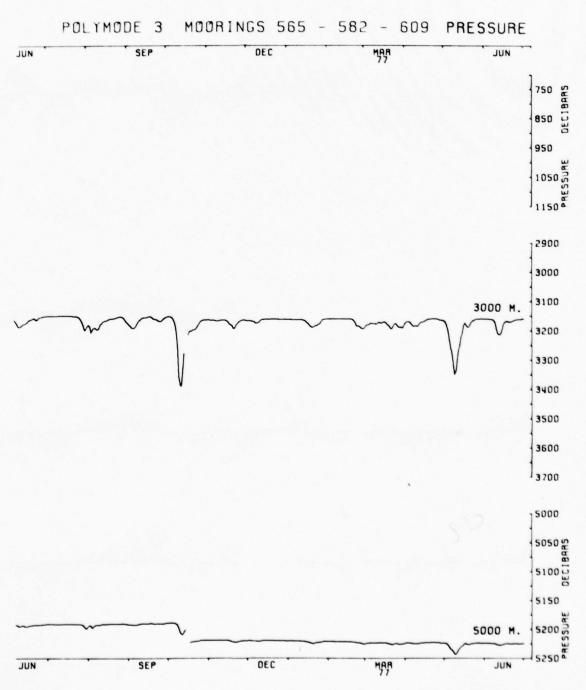
POLYMODE 3 CONTINUED



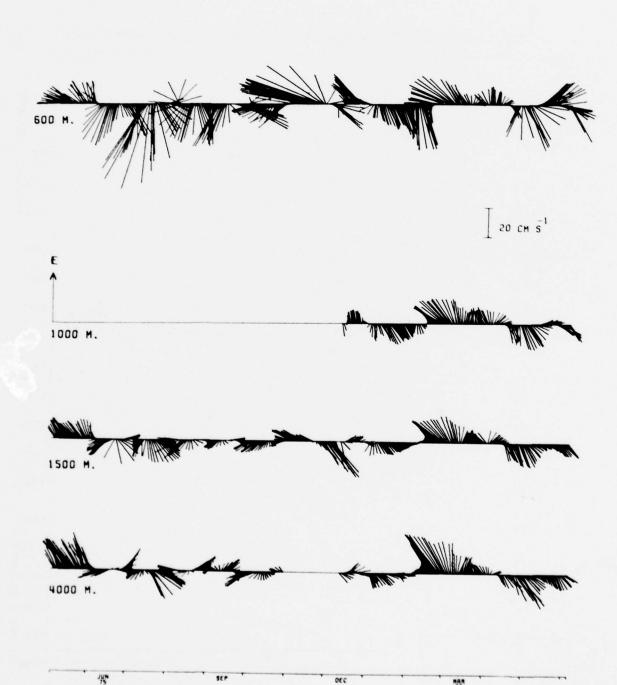




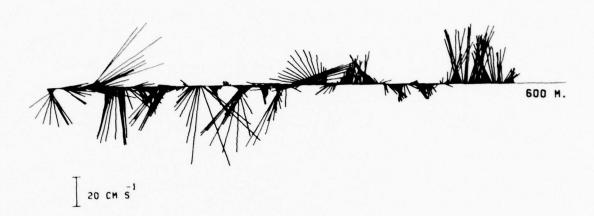




POLYMODE 4 MOORINGS 559 - 578 - 601 CURRENT VECTORS

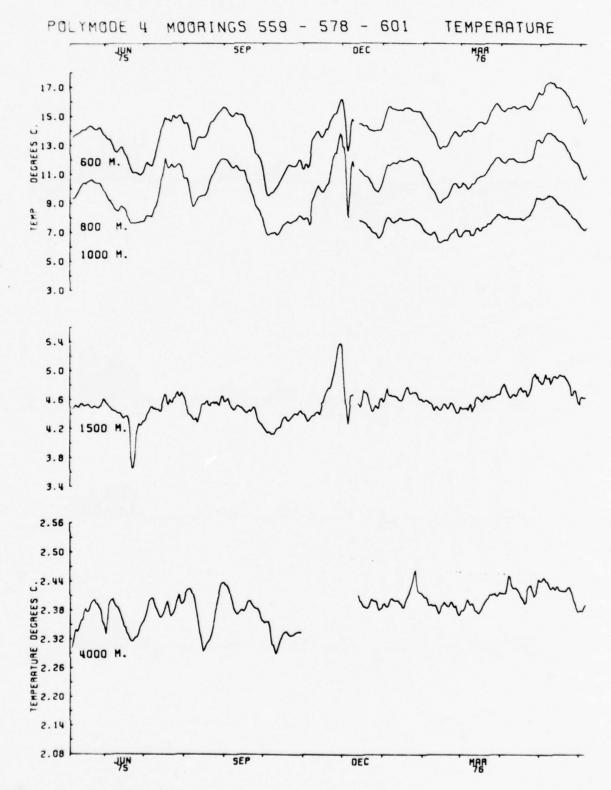


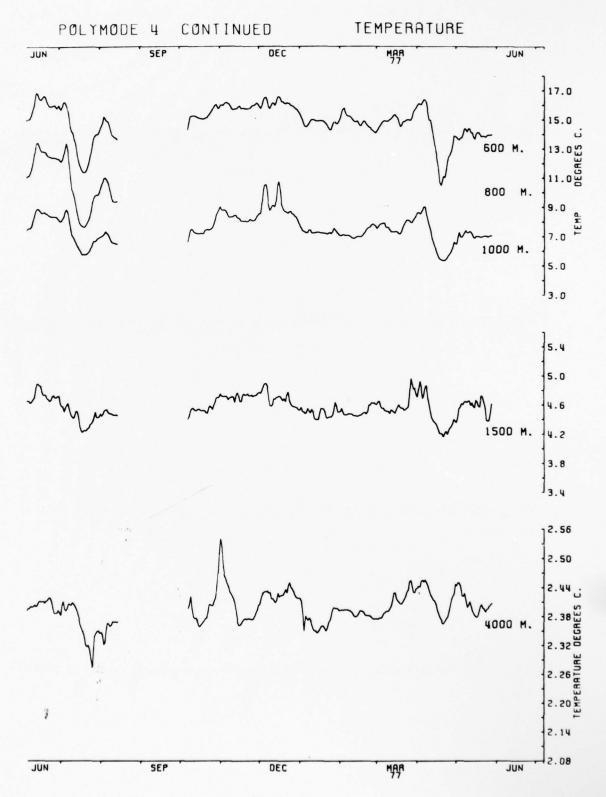




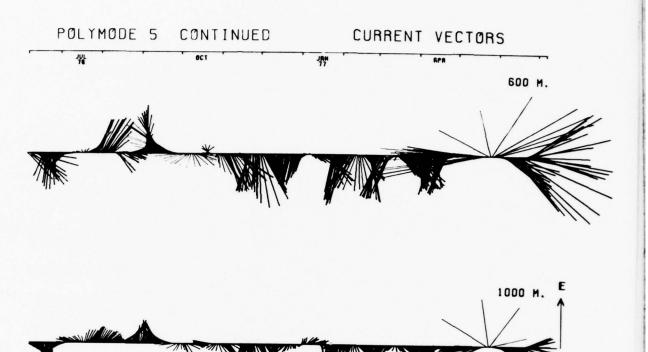






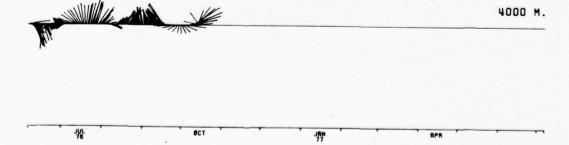


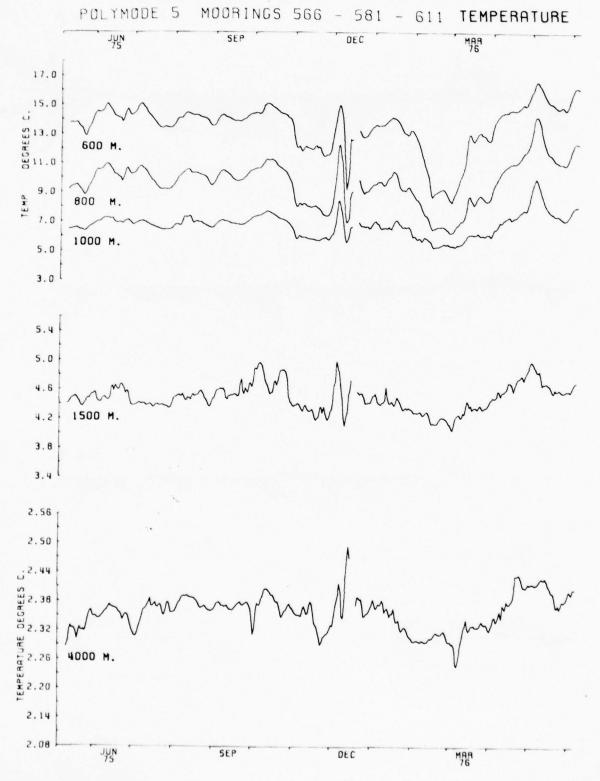
POLYMODE 5 MOORINGS 566 - 581 - 611 CURRENT VECTORS 1500 M. 20 CM 5 4000 M.

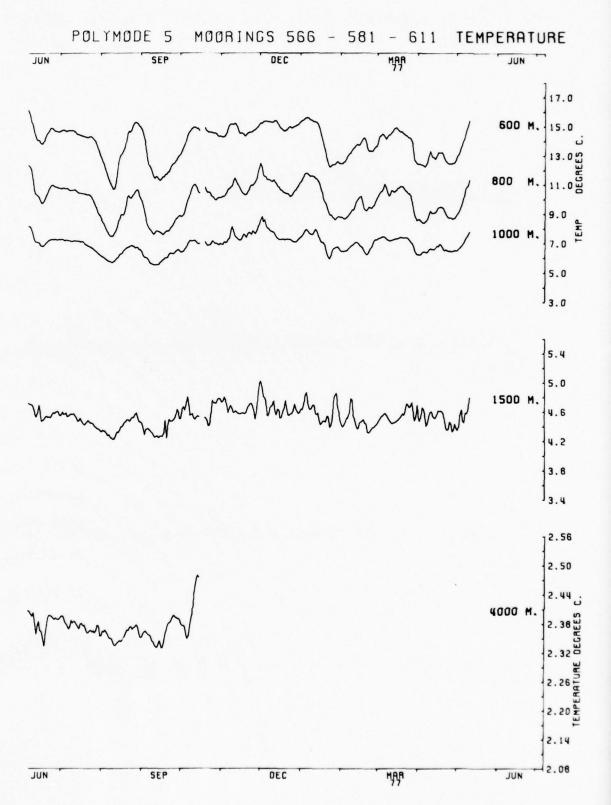


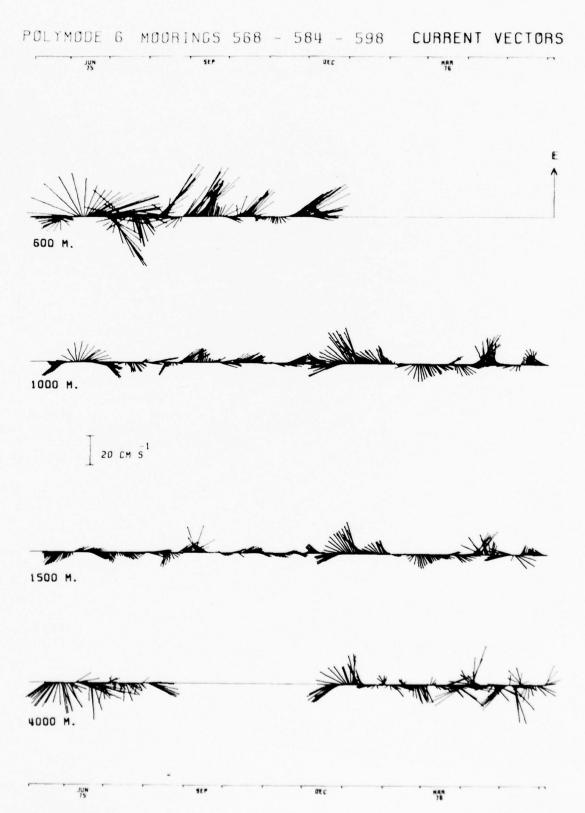


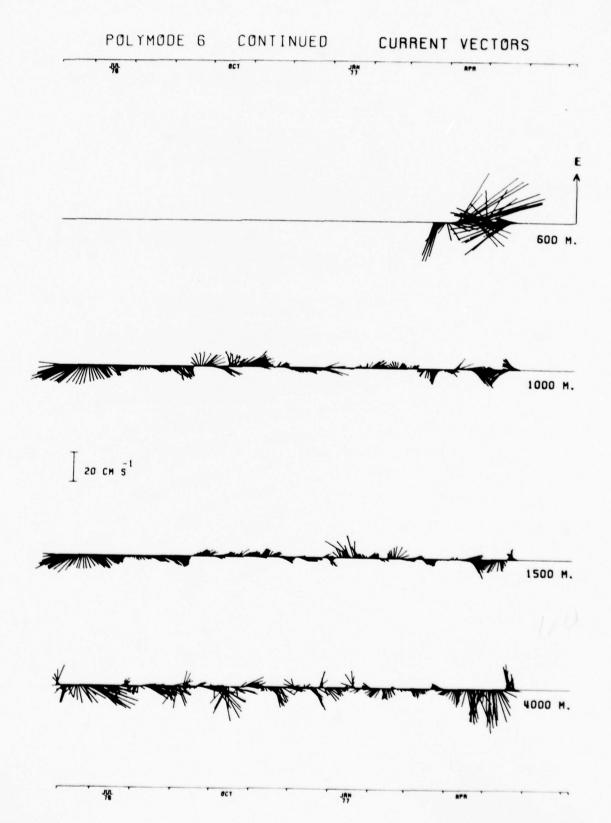
20 CM 51

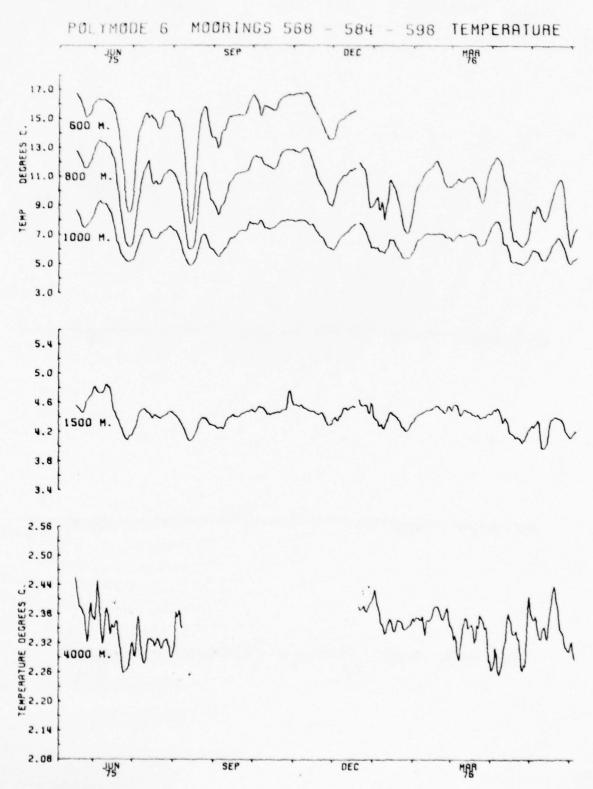


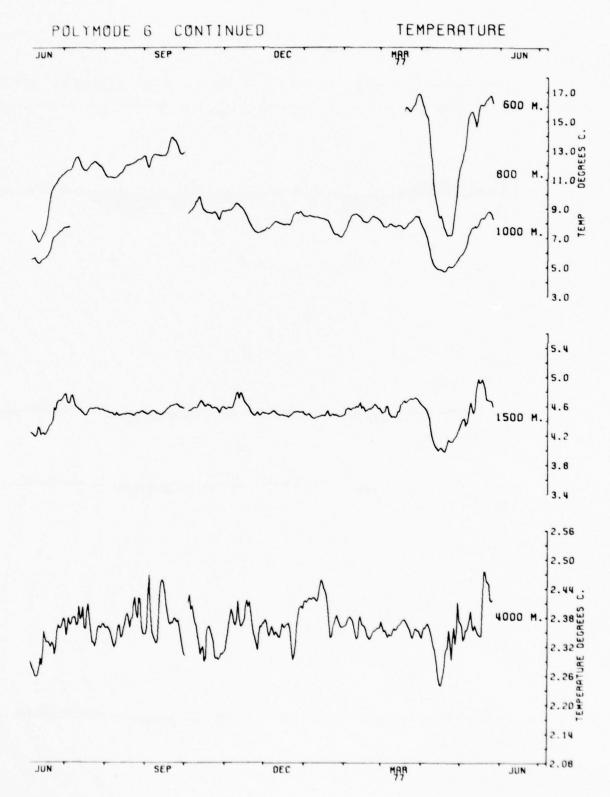


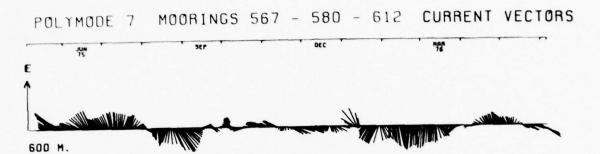


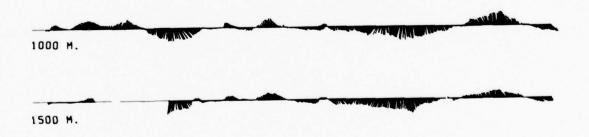




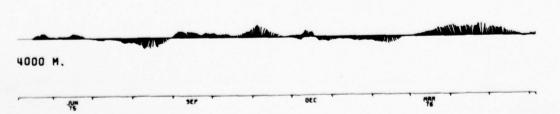


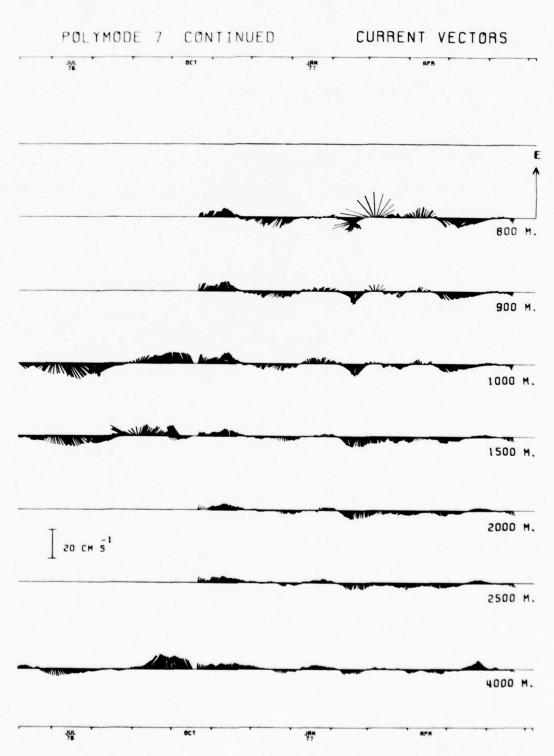


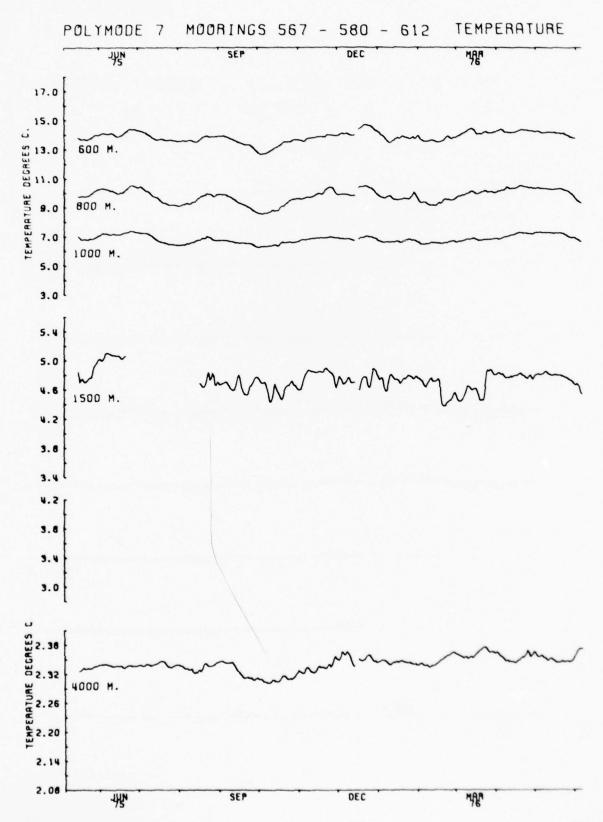


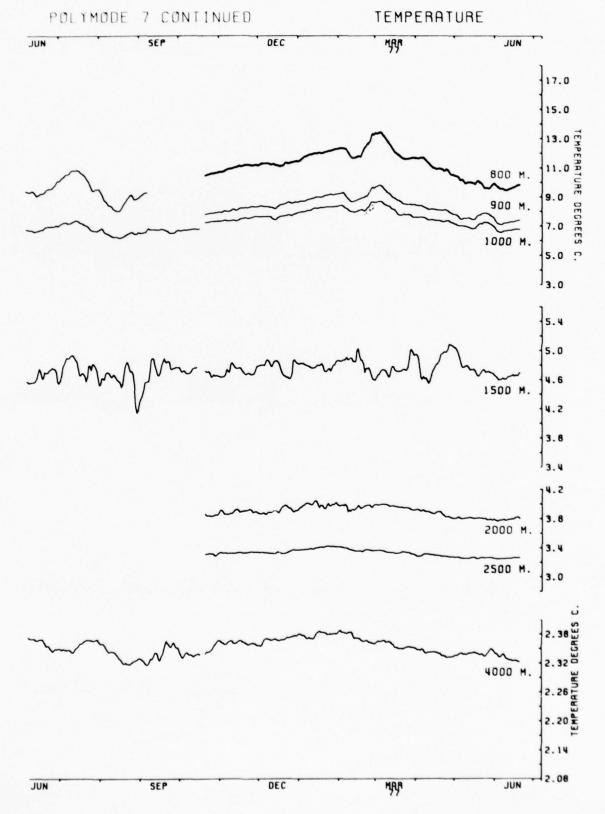




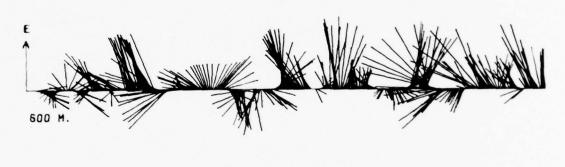








POLYMODE 8 MOORINGS 564 - 577 - 606 CURRENT VECTORS





20 CM 51



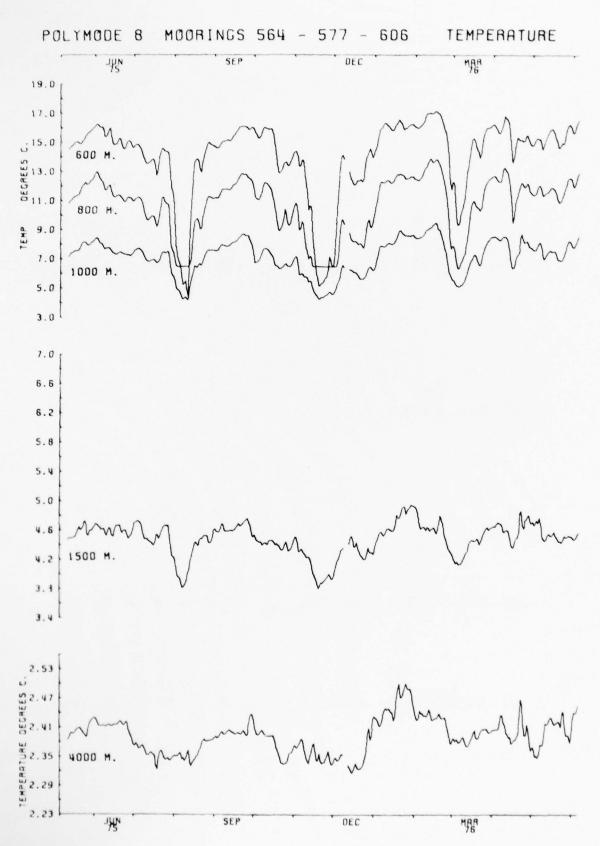


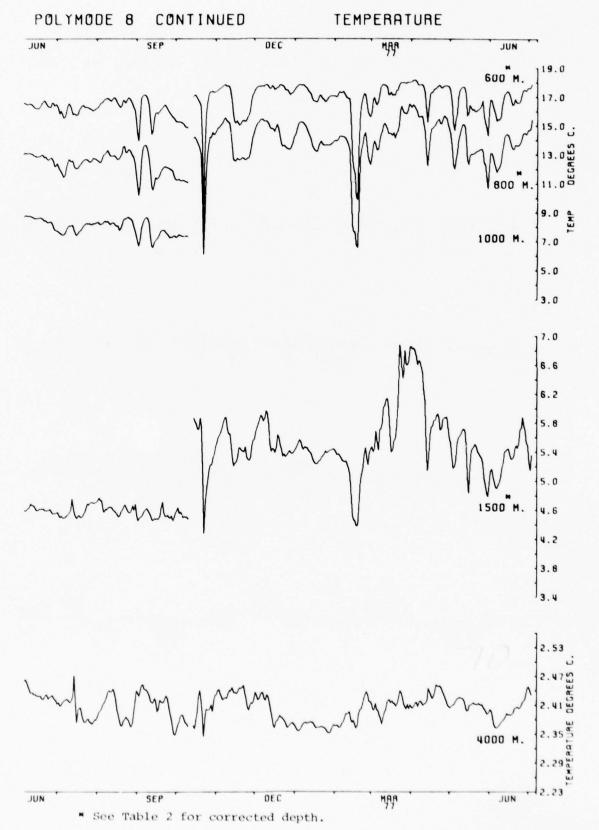
POLYMODE 8 MOORINGS 564 - 577 - 606 CURRENT VECTORS







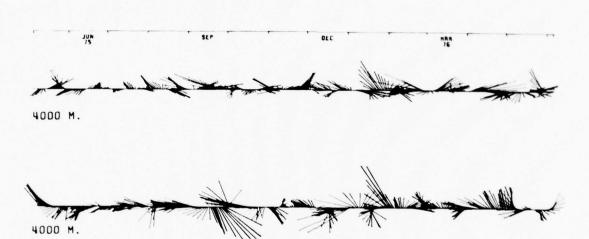




POI	YMODE	12	MOORINGS	560	573 -	605	
POL	YMODE	1.1	MOORINGS	561	574	603	
POL	TMODE	10	MOORINGS	562	575 -	604	

POLYMODE 9 MOORINGS 563 - 576 - 605

CURRENT VECTORS







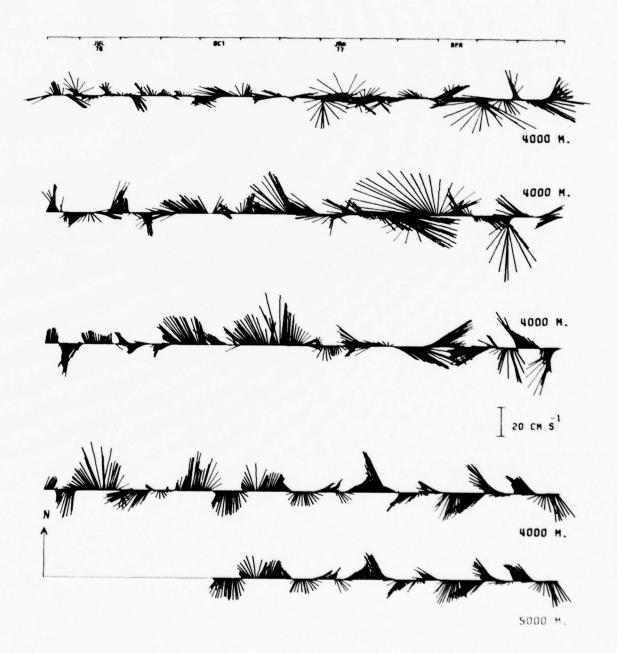
POLYMODE 12 MOORINGS 560 - 573 - 602

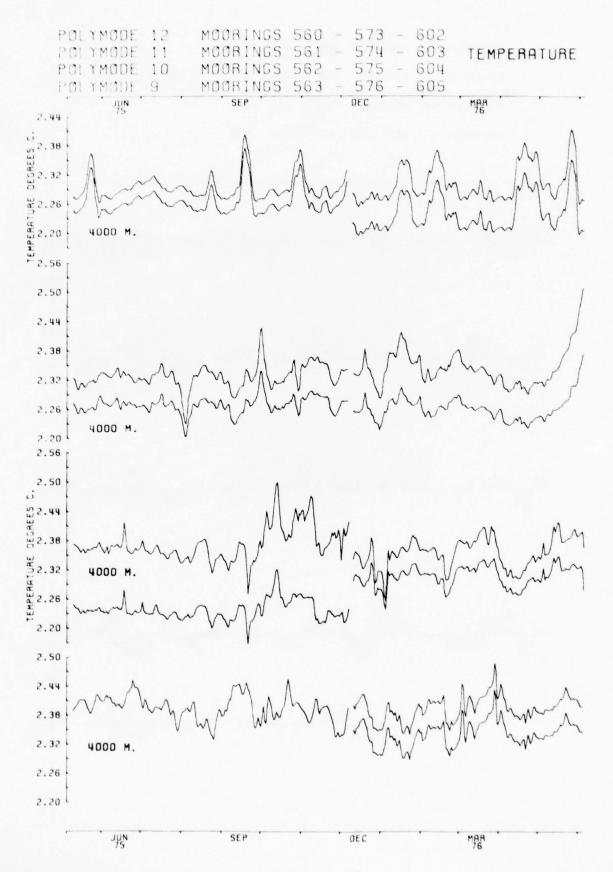
POLYMODE 11 MOORINGS 561 - 574 - 603

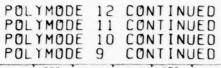
CURRENT VECTORS

POLYMODE 10 MOORINGS 562 - 575 - 604

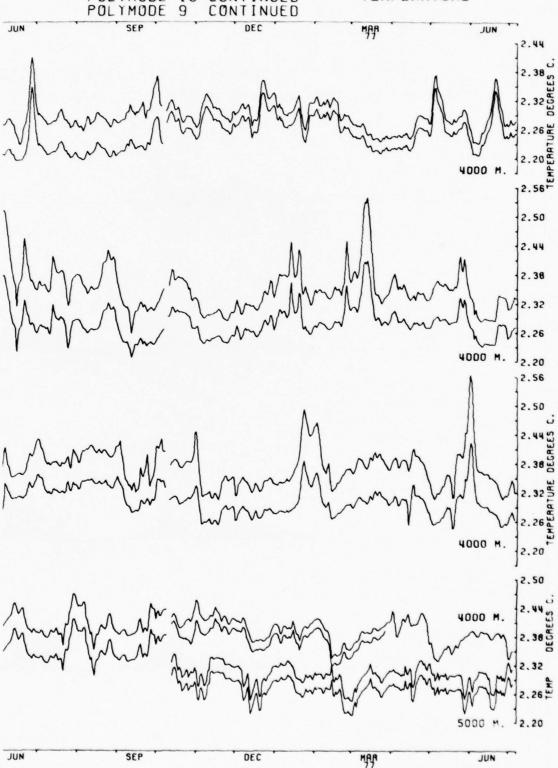
POLYMODE 9 MOORINGS 563 - 576 - 605

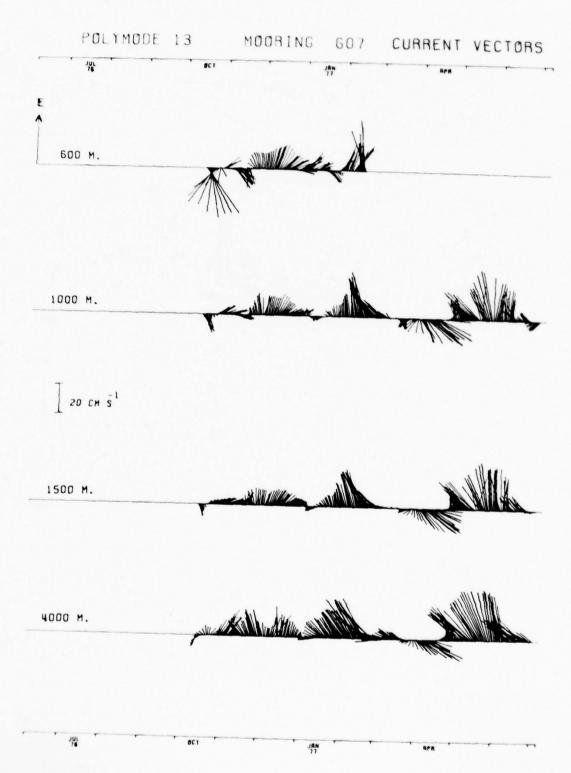


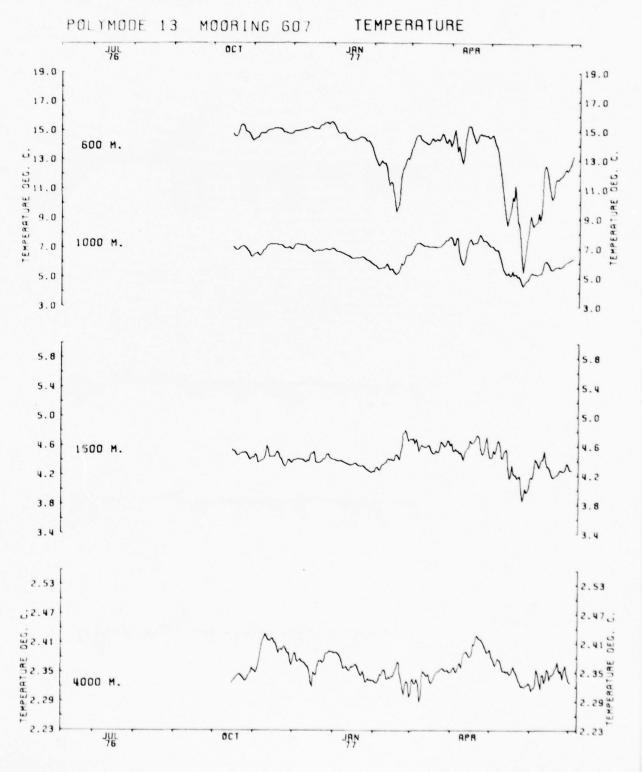


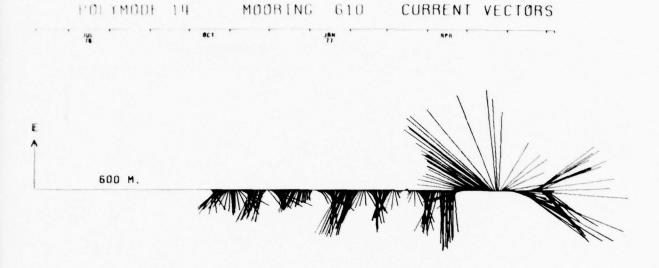


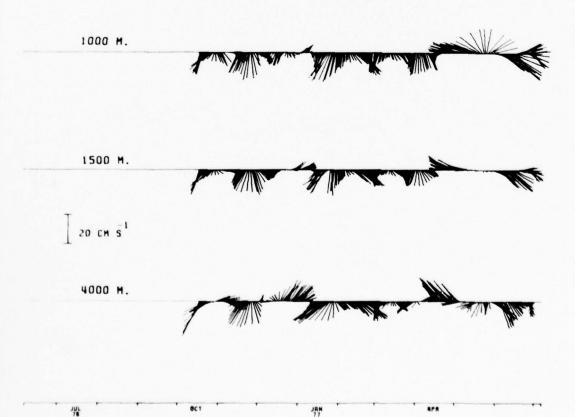
TEMPERATURE

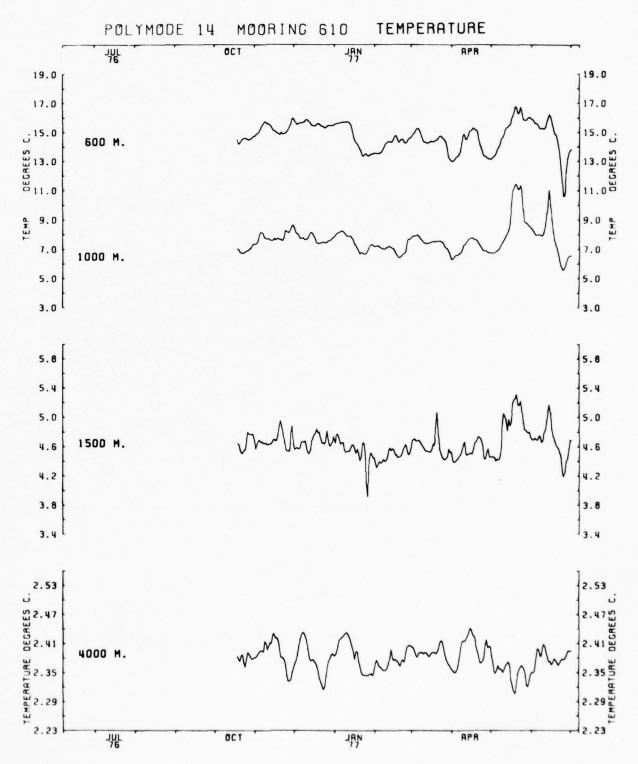




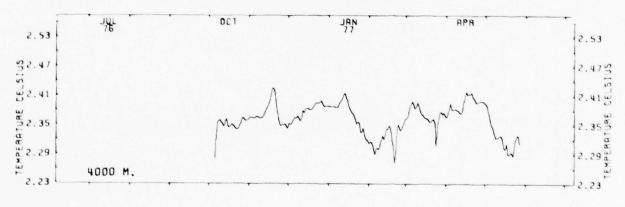


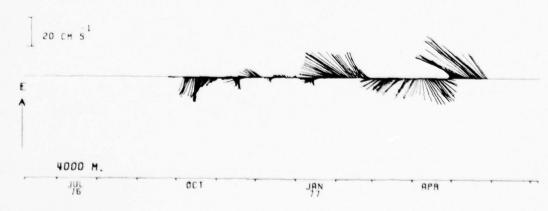


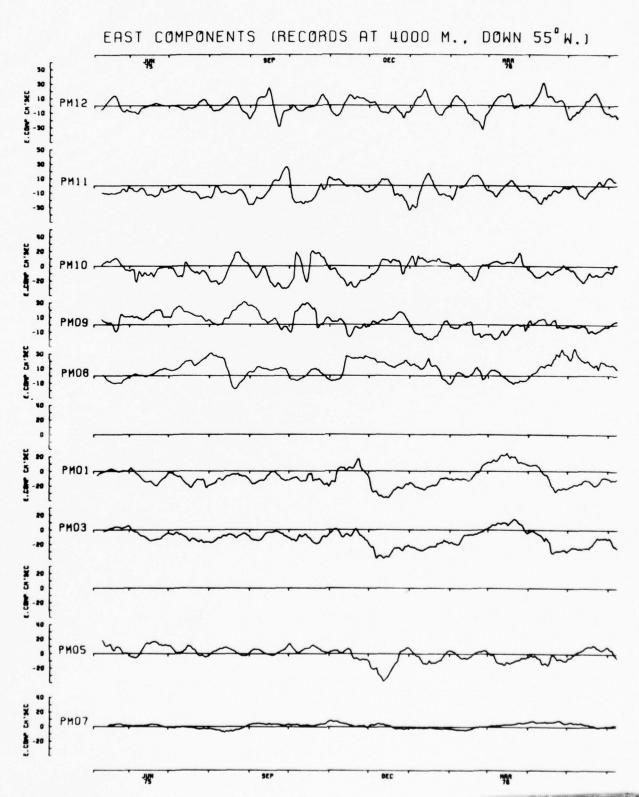


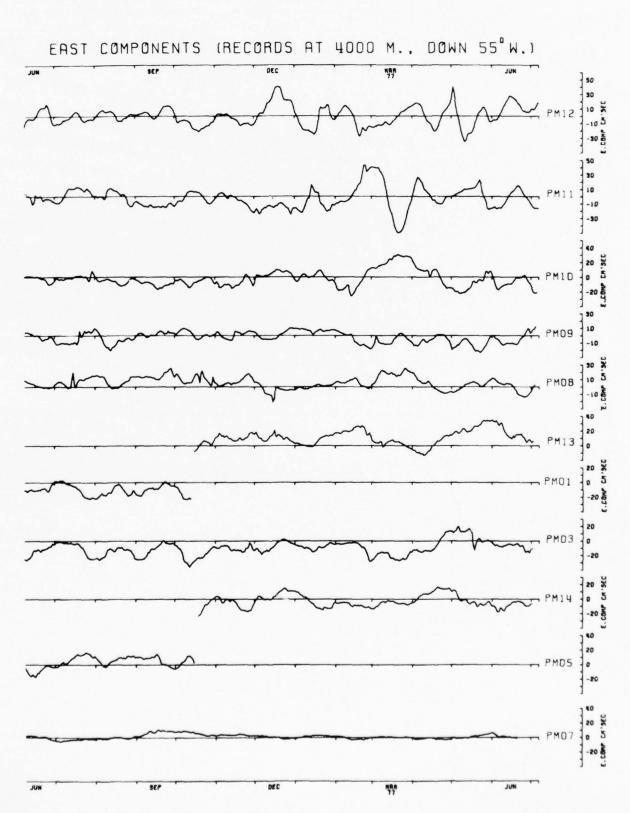


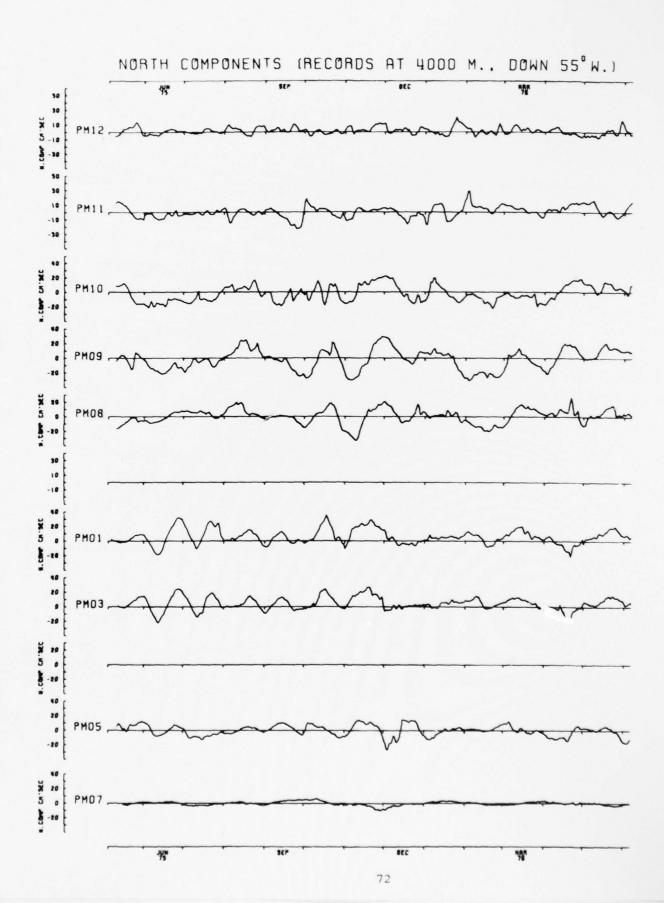
POLYMODE 15 MOORING 599

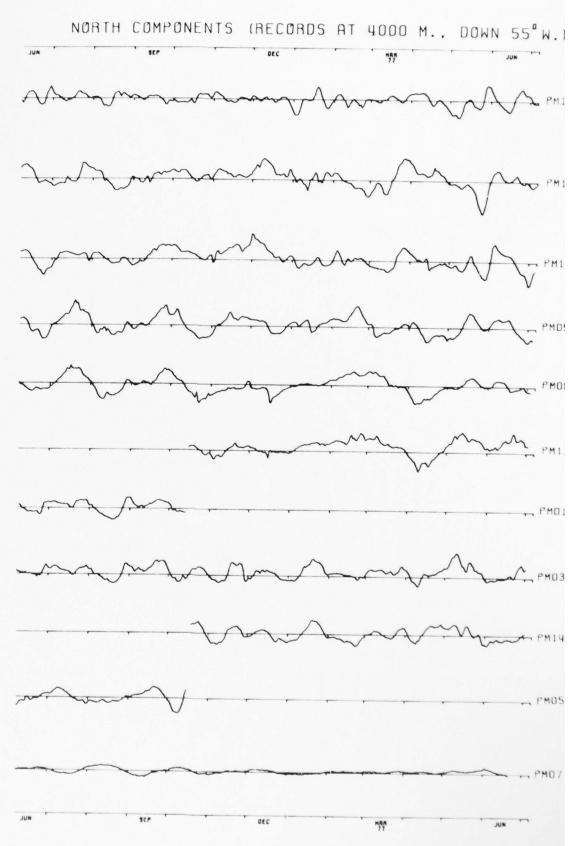












1975 V -18 | V -25 | VI -01 | VI -08 VI -15 VI -22 VI -29 1 VII-06 AT 600 MOORINGS 1,2,3,4,5,8 MOORINGS 1,2,3,4,5,8 AT 1000 M 0 100 0 400 AT 1500M MOORINGS 1.2.3.4.5.8 0 L00 0 400 AT 4000 M MODRINGS 1.2.3.4.5.8

74

0 100 0 400 KM MM/3

1975 VII-13	V11-20	VII-27	VIII-03	VIII-10	VIII-17	VIII-24	VIII-31
600M	VII-20	VIII-PI	VIII-88	VIII-10	77 - 17 - 17 - 17 - 17 - 17 - 17 - 17 -	P3111-24	V)1)-5(
1000M	V11-10	VII-EI	VIII-8	P7117-18	VIII-39	VIII-M	VIII-51
1500M	VII-50	V[1-27	V111-03	VIII-10	VI(I-17	V111-24	V111-51
	W.	41	7.	3.1	11.	2.	4.
4000M	V11-20	VII- 27	W111-89	VIII-10	VIII-17	VIII-N	VIII-31
7	+	>,	7	7 7	<i>\</i> ,	- - -	4.

	0	7	-
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!X -07	IX -14	IX -21	IX -28	X -05	X -12	λ -19	X -26

600M

x -07	1x -14	1x -21	1x -24	x -09	X -12	X -19	X -26
1		_		,	-	~	
		1	,	1 1	1		
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•			1	141		_	\

1000M

x -07	1X -14	1x -21	1X -26	X -05	X -12	X -10	X -26
1	1	-		/	-	1	_
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•	1	,		111	_		

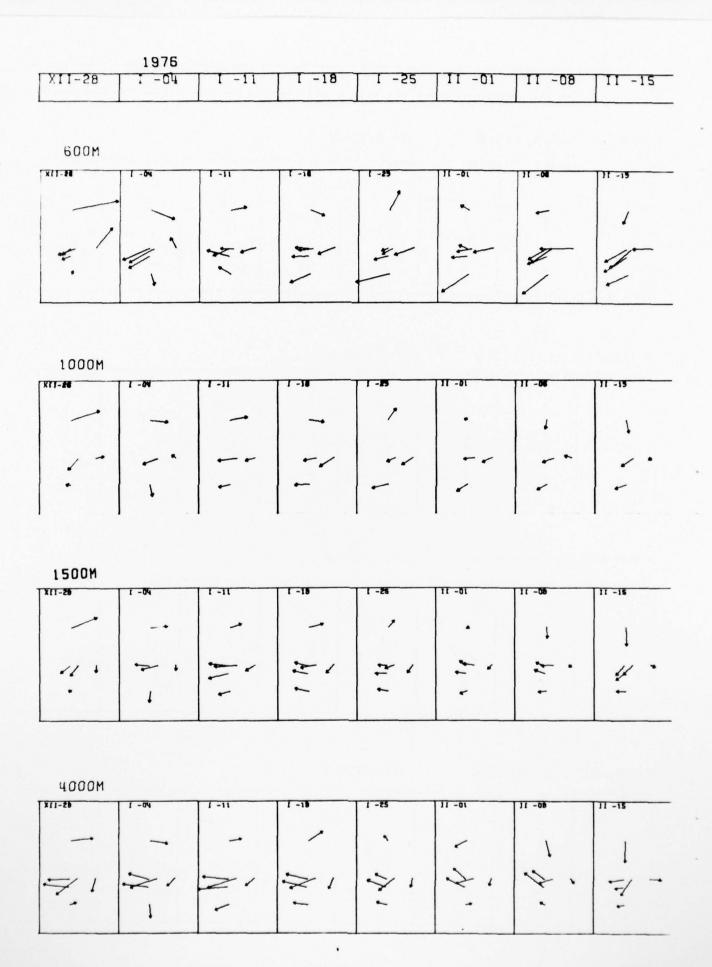
1500M

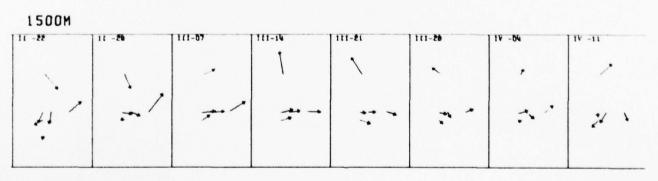
1X ~14	IX -SI	1X -S9	x -05	X -12	X -19	x -26
,	- ,	\	1	\	1	
4.	2,1	7.	41	>,	7.	7.
	,					

4000M

1X -07	1x -14	1x -21	1x -59	x -05	X -12	X -19	X -56
-	-	-		1	1	. /	
> 1	1 + -	=/ 1		-1	4.	7.	> 1
,	1	1	7	7	,	-	-

1979							
XI -05	XI -09	XI -16	X! -23	XI -30	X11-07	XII-14	X11-21
MOORINGS	1,2,3,4,5	5,8	AT 600	м			
X1 -82	XI -60	NT -18	XT -25	XI -30	X11-87	311-14	XTT-FL
11	: /	7		1	<i>j</i> /.		\(\frac{1}{4} \)
MOORINGS			AT 1000				
XI -02	XI -60	XI -18	XI -25	X1 -30	X11-87	XTY-14	XIY-PI
/					/		
,	1,	11	11	7/	2		
14		,	,		/	•	<
MOORINGS	1,2,3,4,5		AT 1500	М			
xt -0\$	x1 -00	XI -16	xt -29	XI -50	X11-07	Xt1-14	X11-5/
/		-		/	/	•	-
1	<i>‡, 7</i>	777	√1 + \	+	>/ ·	-	7,
MOORINGS	1,2,3,4,5	5,8	AT 4000	М			
X1 -02			X1 -29	X1 -90	X11-07	XII-14	XII-EL
1			7	/	/	\	-
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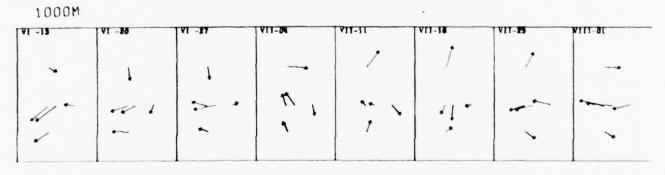


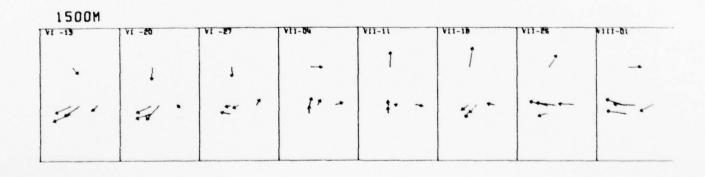


1 -22	11 -29	111-67	111-14	111-51	111-59	1V -04	1V -11
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	1	1	-	-	-	1	/

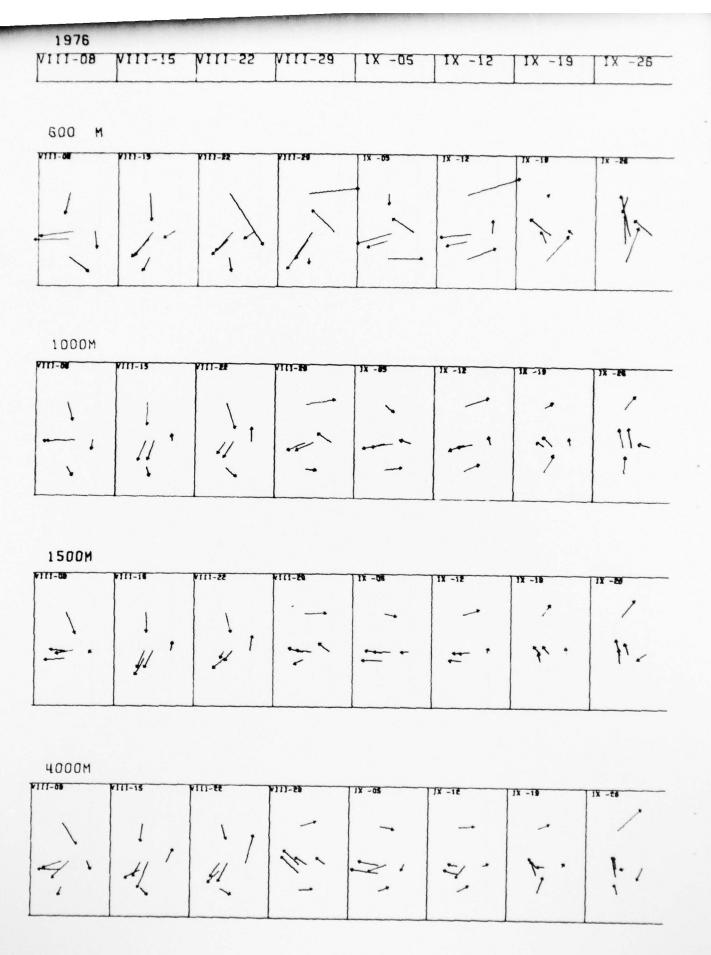
1976 IV -18	IV -25	V -02	V -09	V -16	V -23	V -30	VI -06
MOORINGS	1,2,3,4,	5,8	AT 600	M V - 18	V -25	V - \$8	Vt -Ne
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Ţ.,	7	1.	: 1	!	1//	1-1	1
MOORINGS	1,2,3,4,	5.8	AT 1000	M V -31			
/		-		/	V-8	V- N	VI -04
1.			~ 1	.,	11 ,	• • •	1/
	1,2,3,4,		AT 1500N				
IV -18	1V -H	A ~05	V -010	V -18	V-8	V -90	VI -58
4-	=-	7/	71	1,	h.	21	21
	1,2,3,4,		AT 4000	м			
IV -18	JV -85	v -62	V -09	V -16	V-8	V -50	VI -06
4,-	4.	7/	<i>⇒</i> /	À.	+.	<u>۷</u> -	>,

VI -20	VI -27	V11-04	VII-II	VII-18	VII-25	VIII-01
VI -20	VI -27	VII-84	TVII-II	V11-18	VII-25	וזויש.
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~· 1.	1	11	17	1.	1	
	VI -20			VI -20 VI -27 VII-04 VII-11	VI -20 VI -27 VII -54 VII -11 VII -13	VI -20 VI -27 VII -50 VII -11 VII -18



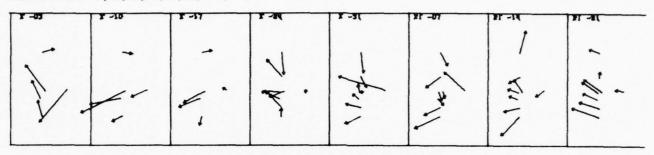


1 -13	V1 -50	VI -27	V11-84	VII-11	VII-18	VII-ES	111-91
\	1	1	-•	1	1	1	-
4.	21 -	> 1	1./	2/	-	2-	=
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X -03 X -1	0 X -17	X -24	X -31	XI -07	XI -14	XI -21

MOORINGS 1,2,3,4,5,8,13,14 AT 600 M



MOORINGS 1,2,3,4,5,8,13,14 AT 1000 M

1-65	¥ -10	8 -57	1-4	1 -9(BE -07	21 -14	Fr -8(
>			= -	:1-	1	4	1114.

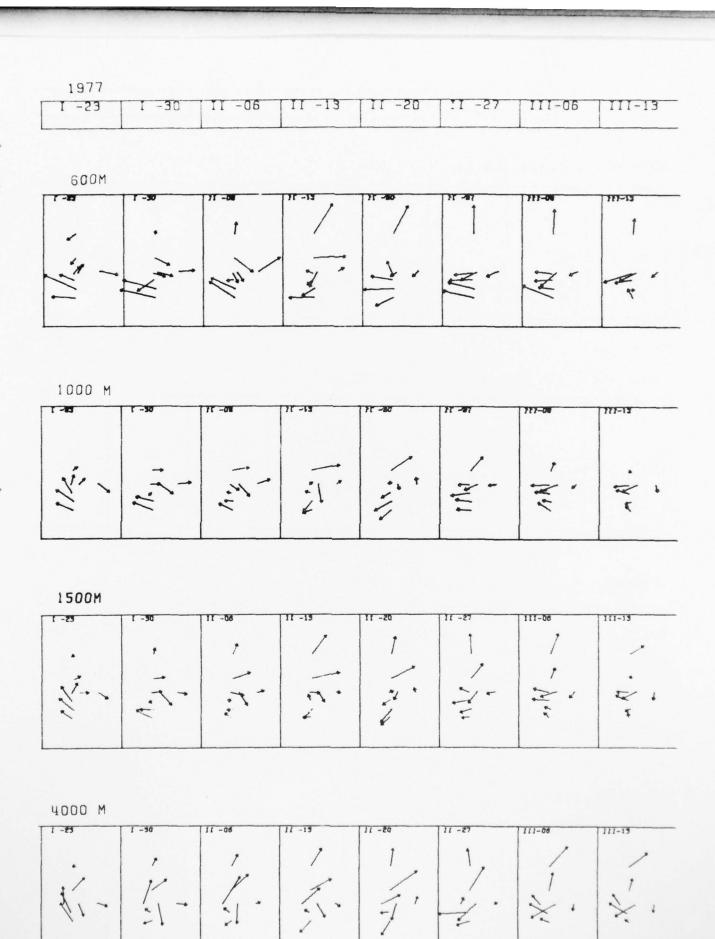
MOORINGS 1,2,3,4,5,8,13,14 AT 1500M

X -05	X -10	X -17	X -24	X -91	X1 -07	XI -14	XI -51
1		\			1	-	
=/	=	=	17	3	1/2 1	= 1	1200
				•	1	1	-

MOORINGS 1,2,3,4,5,8,13,14 AT 4000 M

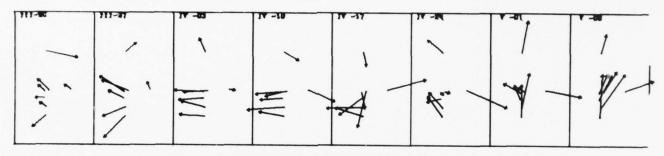
X -05	X -10	x -17	x -24	X -31	XI -07	XI -1X	XI -21
1	-	\		\	1		
4/	7.	~ `	*,	-/-	77	21	3
1	\				'//		

XI -28	X!1-05	XII-12	X11-19	XII-26	1977 I -02	1 -09	I -15
600 M	Fi)-55] N13-18	1307-13) X13-34	T - 012	T ~ 88	17-10
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1000 M	B11-00	#17-1E	¥17-15	HIZ	1-4	T-0	1-14
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4000M	XII-05	XIJ-18	X11-19	X11-56	1 -02	f-05	1-18
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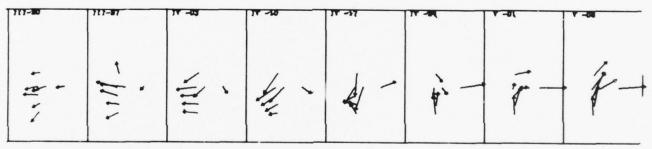


1111-50	111-27	IV -03	IV -10	IV -17	IV -24	V -01	V -08

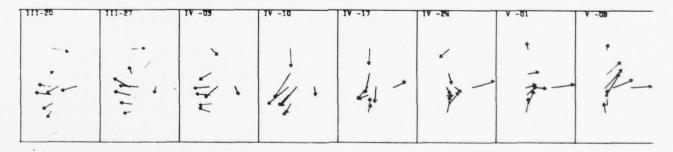
MOORINGS 1,2,3,4,5,8,13,14 AT 600 M



MOORINGS 1,2,3,4,5,8,13,14 AT 1000 M



MOORINGS 1,2,3,4,5,8,13,14 AT 1500M



MOORINGS 1,2,3,4,5,8,13,14 AT 4000 M

111-50	111-87	JV -03	JV -10	JV -17	JV -84	V -01	V -08
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WOODS HOLE OCEANOGRAPHIC INSTITUTION MASS
A COMPILATION OF MOORED CURRENT METER DATA AND ASSOCIATIED OCEA--ETC(U)
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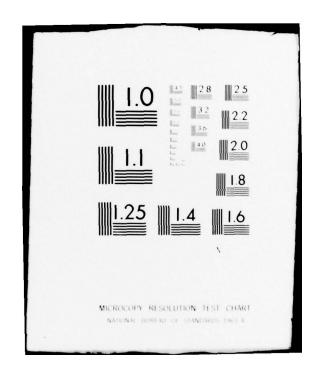


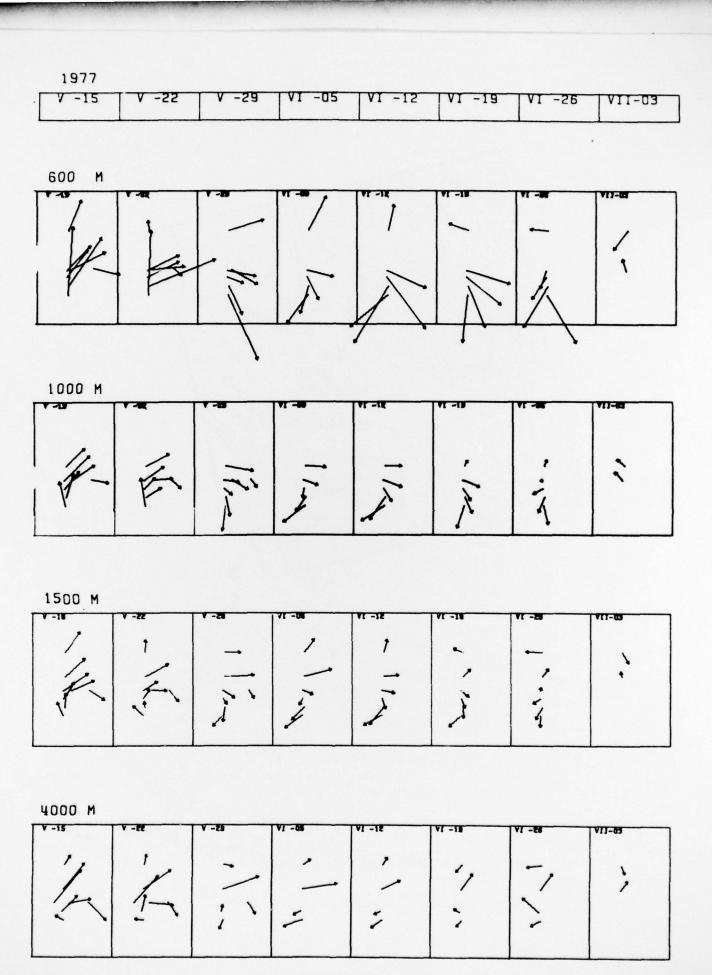


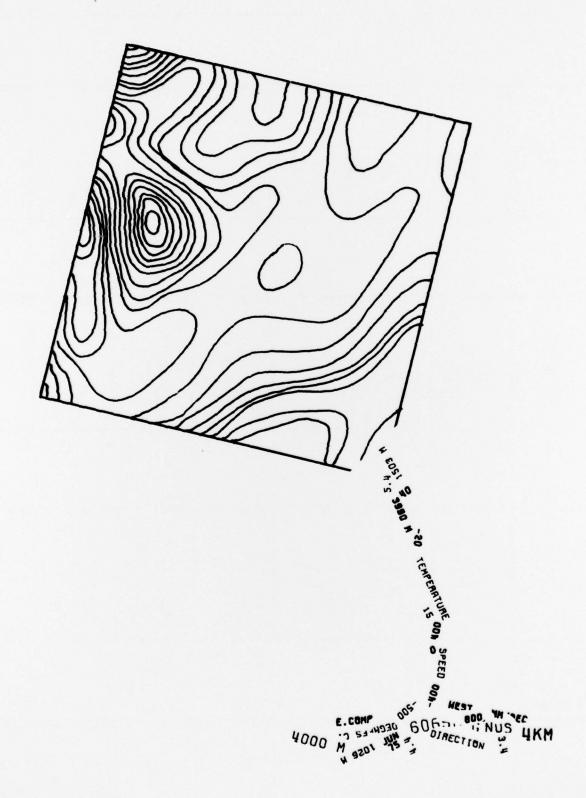




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Spencer, Ann Spencer, Ann NR 083-004 OCE 75-03962 OCE 75-03962 1. POLYMODE POLYMODE IV. . 11. III. IV. Low passed east and north current components, temperature and pressure from current meters and temperature forestern recorders are displayed graphically and in tabular form. Spectral disprass are plotted for temperature and the vector components when a continuous included for relocity data. Low passed east and north current components, temperature and displayed (from current metrs) and temperature from current from current metrs and temperature forms. Spectral disprass are plotted for temperature and the vector components when a continuous included for wholety data. Progressive vector plots are included for wholety data. Summaries of observations from moored stations and CTD profiles taken during POLMODO Array III are presented. Data series of teamly-seven months duration at 12 locations were achieved with 3 consecutive deployments. 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